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Research paper

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Highlights

1. The discrepancy between the PMV and AMV in a well-controlled environment was observed;
2. People's long-term living experience in the hot-humid climate accustoms thermal sensation to warm;
3. Habituations neutralises thermal sensation due to moderated thermal sensibility of the skin;
4. A revised PMV_a are proposed as $PMV_a = 0.22PMV^2 + 0.45PMV - 0.1$
5. PMV_a contributes to the thermal engineering solutions in terms of energy efficiency of an air-conditioning system.

Acronyms	MST	mean skin temperature (°C)	
	P	probability in Hypothesis Testing	
AMV	actual mean vote	PMV	predicted mean vote
ANOVA	analysis of variance	SET*	standard effective temperature (°C)

Abbreviations	PMV _a	adaptive predicted mean vote	
A	body surface area (m ²)	R	heat or lost by radiation (W/m ²)
C	heat lost by convection (W/m ²)	T _{back}	skin temperature of back (°C)
c _b	specific heat of blood [J/(kg•°C)]	T _c	core temperature (°C)
c _c	specific heat of core [J/(kg•°C)]	T _o /dt	rate of change in core temperature (°C/s)
c _s	specific heat of skin [J/(kg•°C)]	T _{calf}	skin temperature of calf (°C)
E _{dif}	heat of vaporized water diffusing through the skin (W/m ²)	T _{chest}	skin temperature of chest (°C)
E _{res}	heat loss by respiration (W/m ²)	T _{forehead}	skin temperature of forehead (°C)
E _{rsw}	heat loss by regulatory sweating (W/m ²)	T _{hand}	skin temperature of dorsal hand (°C)
K	heat conductance of skin tissue [W/(m ² •°C)]	T _{lower arm}	skin temperature of lower arm (°C)
M	metabolic rate (W/m ²)	T _s	skin temperature (°C)
m _c	mass of core (kg)	T _s /dt	rate of change in skin temperature (°C/s)
m _s	mass of skin (kg)	T _{thigh}	skin temperature of thigh (°C)
M _{shi}	metabolic heat by shivering (W/m ²)	T _{upper arm}	skin temperature of upper arm (°C)
		V _b	rate of skin blood flow[kg/(m ² •s)]

Abstract

This paper aims to critically examine the application of Predicted Mean Vote (PMV) in an air-conditioned environment in the hot-humid climate region. Experimental studies have been conducted in a climate chamber in Chongqing, China, from 2008 to 2010. A total of 440 thermal responses from participants were obtained. Data analysis reveals

that the PMV overestimates occupants' mean thermal sensation in the warm environment ($PMV > 0$) with a mean bias of 0.296 in accordance with the ASHRAE thermal sensation scales. The Bland-Altman method has been applied to assess the agreement of the PMV and Actual Mean Vote (AMV) and reveals a lack of agreement between them. It is identified that habituation due to the past thermal experience of a long-term living in a specific region could stimulate psychological adaptation. The psychological adaptation can neutralize occupants' actual thermal sensation by moderating the thermal sensibility of the skin. A thermal sensation empirical model and a PMV-revised index are introduced for air-conditioned indoor environments in hot-humid regions. As a result of habituation, the upper limit effective thermal comfort temperature SET* can be increased by 1.6°C based on the existing international standard. As a result, a great potential for energy saving from the air-conditioning system in summer could be achieved.

KEYWORDS: Thermal comfort, adaptation, PMV, Skin temperature, Hot-humid region, Air-conditioned environment.

1. Introduction

The Predicted Mean Vote (PMV) developed by Fanger is a commonly used index to assess occupants' thermal comfort which has been referenced in international standards including ISO 7730 [1], ASHRAE 55 Standard [2], EN 15215 [3] and Chinese Standard [4]. It is based on the principle of steady-state heat balance and predicts the mean value of the votes of a large group of persons on the 7-point thermal sensation scale (cold (-3), cool (-2), slightly cool (-1), neutral (0), slightly warm (1), warm (2), hot (3)) by six inputs (air temperature, mean radiant temperature, air speed, humidity, metabolic rate and the insulation of the clothing) [5]. In the HVAC engineering design practice, PMV is expected within ± 0.5 to meet 90% occupant satisfaction criteria for indoor thermal environment [1-4]. However the PMV has been challenged by the adaptive thermal comfort principle from field studies and has been criticized as over/under estimating occupants' actual thermal sensation, i.e. Actual Mean Vote (AMV) [6, 7]. Research into adaptive thermal comfort first began following the oil crisis in the mid-70's [8] and has increased dramatically in recent years due to the concerns over climate change and energy efficiency.

It has been concluded that behavioral, physiological and psychological adaptation processes are the three types of presumed causes of the discrepancies between the PMV and AMV [6, 9]. However, besides giving a statistical approximation of the general effect of such adaptive processes on the thermal perception vote, little is known about the individual contributions of the three types of adaptive processes to the effect [10]. Liu *et al.* [11] conducted a subjective survey research and introduced a method of quantifying the portions of the adaptation processes by weighting the contribution of these three adaptation categories to the thermal adaptation using the analytic hierarchy process (AHP). However, the specific quantitative identification of each category still remains uncertain.

Principles of adaptive thermal comfort were mainly studied in free-running buildings through field surveys [12-17]. A review of the previous studies reveals that there is little research on the topic of adaptive thermal comfort in air-conditioned environments. For example, de Dear [6] statistically analyzed discrepancies between the PMV and the AMV in air-conditioned environments from the ASHRAE RP-884, a quality-controlled global database. He concluded that ‘adaptation is at work in buildings with central HVAC, but only at the biophysical (behavioral) level of clothing and air speed adjustments’; ‘PMV appears to have been remarkably successful at predicting comfort temperatures in the HVAC buildings of RP-884’s database’. In contrast, Humphrey [18] analyzed the *vote bias*, PMV minus AMV, using the same database. He argued that the possible origins of the bias may be caused by physical, psychological or physiological factors. Humphreys argued that ‘PMV can be seriously misleading when used to predict the mean comfort votes of groups of people in everyday conditions in buildings, particularly in warm environments’. The research leaves open two questions: i) can the PMV predict thermal comfort accurately in air-conditioned buildings and ii), if not, what factors are involved and how do they impact on actual thermal sensation in addition to the behavioral adaptation?

The occupant acceptable indoor temperature is considered as one of the design criteria of an air-conditioning system, which is one of the key factors with impacts on the operation of air-conditioning and therefore the energy consumption of buildings [19, 20]. Currently the international and national standard for design and operation

temperatures of an air-conditioning system is based on the PMV/PPD method [1-4]. The aim of this research is to observe and examine the discrepancies between the PMV and AMV in an air-conditioned environment through a laboratory study, and identify the factors contributing to such discrepancies, consequently provide optimal design basis for the engineering solutions to a creation of thermal environment in hot-humid region.

2. Research Methods

Quantifying the specific factors contributing to the vote bias between the PMV and AMV poses considerable challenges because the factors such as physical environmental parameters, occupant adaptive behavior and their previous thermal experience, and occupant thermal comfort expectations are all variables in real buildings. However, these challenges could be solved in a laboratory study by limiting variables and focusing on one variable in each experimental case. The research methods applied in this study include experimental measurement, a subject questionnaire survey and statistical data analysis. Previous field studies in free-running buildings indicated that occupants demonstrated a strong adaptability, particularly in the hot-humid tropics [6, 21-24]. We carried out laboratory experiments in Chongqing, the region with typical hot and humid climatic characteristics in summer. The typical summer climate condition in Chongqing is listed in Table 1 [25]. The average air temperature in summer is 26.9°C and the average relative humidity is 78%. The climate chamber can provide the required indoor physical environmental parameters including air temperature, relative humidity and air velocity constantly during the experiment. In order to identify the contribution of the physiological and psychological categories, the behavior adaptation was eliminated from the three adaptation categories. The ASHRAE seven-scale thermal sensation surveys were conducted during the experiment period. Statistical methods and Bland-Altman agreement assessment have been applied in data analysis.

Table 1. Typical climate condition in the summer in Chongqing [25]

Month	Air temperature (°C)		Relative Humidity (%)
	Monthly Mean	Maximum	Monthly Mean
June	25.2	34.9	81.2
July	28.0	36.6	77.1
August	27.6	37.7	75.7

2.1 Experiment

Four series of human exposure experiments in the climate chamber were carried out during the summer in the period from 2008 to 2010. In each series, we have recruited 20 subjects from the region. Each series had a number of environmental conditions with various settings. In total, 22 thermal conditions were created in the climate chamber for the experiments, which are listed in Table 2. These conditions represent typical, real-life, warm environments that people usually experience in this region.

Table 2. Experimental setting conditions and measured thermal environment

Experiment Series No.	Setting Conditions—ambient temperature/relative humidity/velocity (°C/%/m·s ⁻¹)	Measured thermal environmental parameters ^b			
		Ambient Temperature (°C)	Velocity(m/s)	Relative Humidity (%)	Black-bulb Temperature (°C)
1	26/70/0.0 ^a	25.9±0.2	0.04±0.01	71±2	25.9±0.2
	27/70/0.05 ^a	27.0±0.2	0.04±0.00	71±2	26.9±0.2
	28/70/0.05 ^a	28.0±0.1	0.04±0.01	70±2	27.8±0.1
	29/70/0.05 ^a	29.0±0.1	0.04±0.00	70±2	28.7±0.1
2	27/50/0.1 ^a	26.9±0.2	0.11±0.02	54±4	26.6±0.1
	29/50/0.1 ^a	28.9±0.2	0.11±0.04	55±7	28.5±0.2
	31/50/0.1 ^a	31.0±0.2	0.14±0.04	51±7	30.4±0.1
	33/50/0.1 ^a	32.9±0.2	0.12±0.02	54±5	32.3±0.1
3	26/40/0.1 ^a	25.6±0.1	0.08±0.05	41±1	25.6±0.1
	26/60/0.1 ^a	25.9±0.1	0.1±0.06	60±1	25.6±0.1
	26/80/0.1 ^a	26.0±0.1	0.06±0.05	80±1	25.6±0.1
	28/40/0.1 ^a	28.0±0.1	0.07±0.01	40±2	27.6±0.1
	28/60/0.1 ^a	27.9±0.1	0.09±0.03	60±1	27.6±0.2
	28/80/0.1 ^a	28±0.2	0.09±0.04	80±2	27.6±0.1
	30/40/0.1 ^a	29.8±0.1	0.1±0.02	42±2	29.4±0.2
	30/60/0.1 ^a	29.9±0.1	0.09±0.03	60±1	29.4±0.1
4	30/80/0.1 ^a	29.9±0.1	0.09±0.05	81±1	29.4±0.1
	28/90/0.1 ^a	28.0±0.1	0.06±0.03	90±1	28.0±0.1
	28/90/0.8 ^a	28.1±0.2	0.79±0.04	90±1	28.0±0.2
	30/80/0.6 ^a	30.0±0.1	0.61±0.02	80±1	30.0±0.1
	30/80/0.8 ^a	30.0±0.2	0.81±0.04	80±1	29.8±0.2
	32/90/0.8 ^a	32.0±0.2	0.79±0.03	80±1	31.9±0.2

^a Numbers of Samples in each dataset are n=20.

^b Values are presented as mean value ± standard deviation.

2.2 Subject characteristics

The 20 subjects in each series are in an age range of 20 to 30 years old. They were recruited randomly to participate in each experiment condition with the gender ratio of 1:1. In total 80 subjects were involved in the experiments and form 440 valuable samples for analysis. All the students were healthy, i.e., not currently taking prescription medication and having had no history of cardiovascular disease. Subjects were asked to avoid caffeine, alcohol, and intense physical activity for at least 12 hours prior to tests. They were briefed on the purpose of the tests, familiarized with experimental procedures and trained to know the test procedure well. During the experiment period, subjects were required to wear a uniform clothing made in the same style with same color and materials in the most fitted size. This uniform clothing had an equivalent insulation level of 0.26clo (1clo equal to $0.155\text{m}^2\cdot\text{K}/\text{W}$) [1] including short-sleeve shirts, shorts and lightweight shoes. All the subjects had been living in Chongqing for over two years at least, thus it is supposed that they had the hot-humid climate thermal experience and hence had generated habituation and/or acclimatization to the specific climate characteristics.

2.3 Experimental procedure

The experiment in each setting condition lasted for 120 minutes. For the first 30 minutes, subjects were asked to change into the uniform clothes and sit quietly in a rest room, next to the climate chamber. This was kept at a temperature of 26°C as a neutral environment. After this period subjects were moved into the climate chamber for a 90 minutes exposure. During the first 30 minutes, the subjects were relaxed and got used to the chamber environment. The actual measurement and questionnaire survey were conducted in the next 60 minutes. During the experiment period the thermal sensation questionnaire survey; skin temperature measurements with 13 locations of the body including forehead, chest, back, upper arm (right and left), lower arm (right and left), dorsal hand (right and left), calf (right and left), and thigh (right and left); and environment measurements were performed simultaneously every 10 minutes. Subjects were given sedentary office activities without any behavioral adaptive actions during the exposure. The ASHRAE thermal sensation scale was used in the questionnaire for quantifying occupant's thermal sensation. This is as follows: -3(Cold), -2(Cool), -1(Slightly cool), 0(Neutral), +1(Slightly warm), +2(Warm), +3(Hot). Figure 1 shows the experiment scene.



Figure 1. Climate chamber experiment scene

2.4 Measurements

For the calculation of PMV and standard effective temperature (SET*), the thermal environmental parameters around the subjects were measured by a Thermal Comfort Monitoring Station (LSI). The LSI was positioned at a height of 0.6m above the floor. All sensor probes for measuring ambient temperature, black-bulb temperature, relative humidity and air velocity were in conformity with the ISO 7726-2001 standard [26]. The specifications of the sensor probes employed in this study are shown in Table 3.

The copper-constantan thermocouples were attached to the different local skin positions to measure the local skin temperatures. All the thermocouples were calibrated using a standard mercury thermometer with a precision of 0.1 °C. These were linked to a multi-channel data collector which recorded the skin temperatures automatically.

Table 3. Ranges and precision of the LSI instrument

Environment parameters	Range	Precision
Air temperature	-25 ~ 150°C	± 0.1°C
Thermal Comfort Monitoring Station (LSI)	Relative humidity	± 2% (15-40%) RH
		± 1% (40-70%) RH
	Air velocity	± 0.5% (70-98%) RH
		±0.05 m/s (0~0.5m/s)
	0.01 ~ 20m/s	±0.1 m/s (0.5~1.5m/s)
Black-bulb temperature	-10~100°C	± 0.15°C

2.5 Calculation and statistical analysis

The PMV and the ASHRAE standard effective temperature (SET^*) were calculated by the standard procedure provided by ISO 7730 [1] and Gagge's study [27] respectively. The average values of the measured thermal parameters in each experiment condition were used as the inputs for the calculation of both PMV and SET^* index. An 8-point weighted method [28] was adopted to calculate the mean skin temperature (MST), as represented by Equation 1.

$$MST=0.07T_{forehead} +0.175T_{chest} +0.175T_{back} +0.07T_{upper\ arm}+ 0.07T_{lower\ arm}+ 0.05T_{hand}+ 0.19T_{thigh}+ 0.20T_{calf} \quad (1)$$

To examine the statistical significance of the experimental data, the analysis of variance (ANOVA) and T-test were conducted using SPSS 20.0 [29].

To investigate the subject's mean responses in experiment conditions, Bin process [6] was conducted by calculating the mean values of subjects' thermal sensation vote and skin temperature in each experiment condition bin (shown in Section 3.2 and 3.3).

The aim of this research, as stated, is to observe the discrepancy between the PMV and AMV in a well-controlled environment and, if it exists, to identify the causation factors. Therefore it is necessary to assess the agreement of the PMV calculated based on the experimental physical parameters and the AMV based on the subjects' simultaneous thermal comfort votes. Bland and Altman proposed a method of assessing agreement between two measurements methods in clinical research. They criticized the commonly-used approaches including 'Comparison of means', 'Correlation coefficient', and 'Regression' as inappropriate ways for assessing the agreement of two different measures [30] and proposed a new approach which was named *Bland-Altman analysis* [31, 32]. Bland-Altman analysis is based on graphical techniques and simple calculations. Zaki [33] endorsed that in medical research the Bland-Altman method was the most appropriate method for agreement assessment between two methods and over 85% of existing studies applied this method. In our study, in order to assess the agreement between PMV and AMV methods, we introduce the Bland-Altman method from medical research to thermal comfort research. The PMV and AMV can be regarded as two methods of measurement of thermal comfort. To apply the Bland-Altman method, we calculated the mean difference (\bar{d}) of the level of thermal comfort

obtained by AMV and PMV methods and the standard deviation of the differences (s_d). Consequently, the degree of agreement, or so called 'limits of agreement' ($\bar{d} \pm 2s_d$), were obtained. The PMV and AMV can be interchangeable only if the provided differences within this 'limits of agreement' are acceptable by professional knowledge. The principles and details of the Bland-Altman analysis can be found in references [31] and [32]. The analysis results are shown in Section 4.1.

3. Results and analysis

3.1 Thermal sensation and SET*

The ASHRAE standard effective temperature (SET*) is defined as the equivalent temperature of an isothermal environment at the relative humidity level of 50% RH in which a subject, while wearing standardized clothing for the activity concerned, would have the same heat stress (skin temperature) and thermoregulatory strain (skin wettedness) as in the actual test environment [27, 34]. The SET* is a comfort index that was developed based upon a two-node dynamic model of the human thermal regulation mechanism.

In this study, the SET* and PMV for each experiment condition were calculated based on the physical parameters recorded. The subjects' actual mean thermal sensation votes, referred to as the Actual Mean Vote (AMV), for each experiment condition were recorded through the subject questionnaire survey during the experiment period. Figure 2 shows the relationship of AMV against SET* in four series of experiments respectively in comparison with the PMV, and each dot in the figure represents the mean value in a certain condition with 20 samples. This figure reveals that the mean thermal sensation vote increases when the SET* increases. In addition, there are discrepancies between PMV and AMV. PMV generally overestimates the subjects' actual mean thermal sensation. Moreover, in most series, PMV has a high significant linear relationship with SET*($P < 0.001$), but AMV tends to follow a non-linear relation with SET*, especially in warmer conditions.

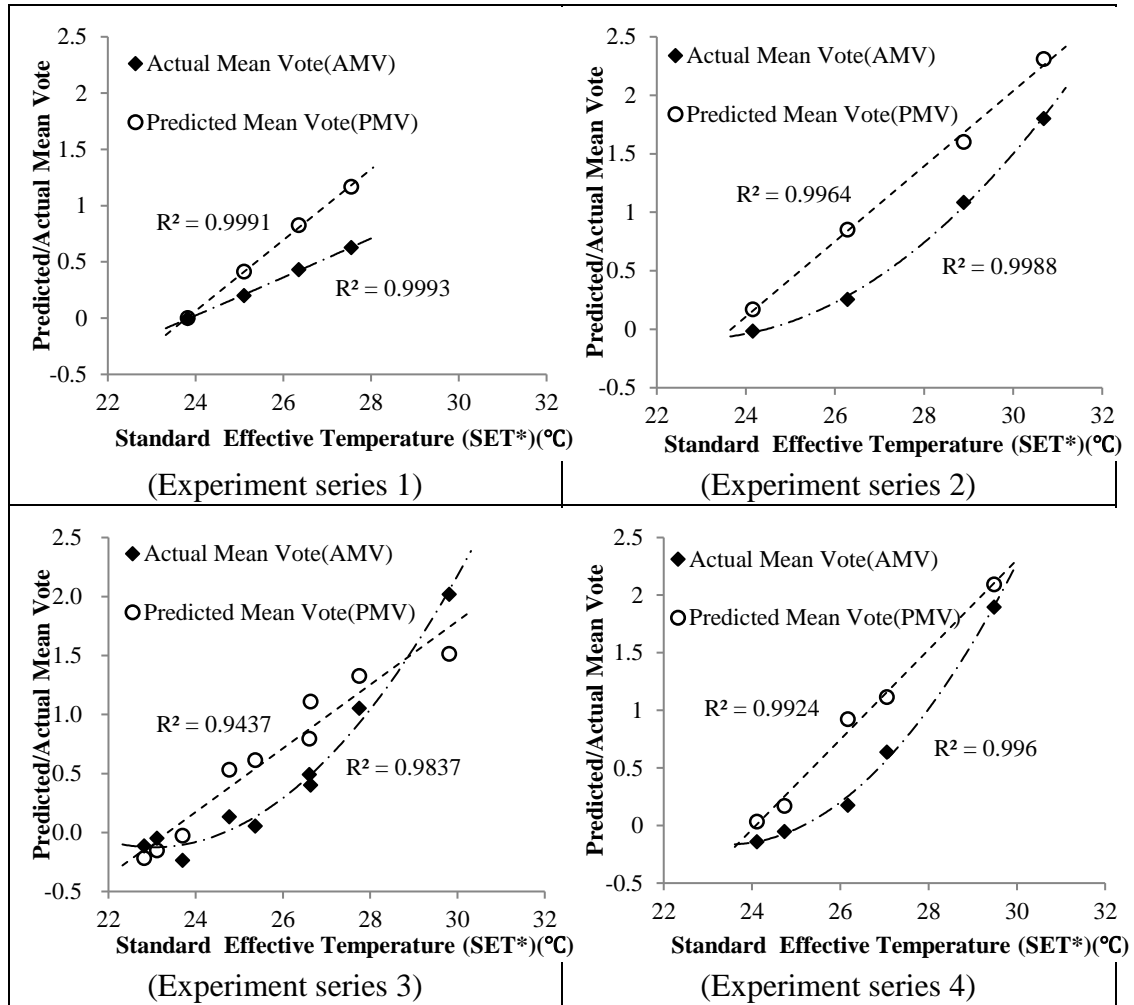


Figure 2. Thermal sensation vote (PMV and AMV) against SET* in each experiment series described in Table 1

We plotted all the data collected from the four series in Figure 3 to present the relationships of the thermal sensations (PMV and AMV) against the SET*. From the figure we can see that PMV has a linear relation with SET*, while the AMV has a polynomial relation fit with SET*. The regressions of PMV/AMV against SET* were at the temperature range of $23^{\circ}\text{C} < \text{SET}^* < 33^{\circ}\text{C}$. The correlations can be expressed by Equations 2 and 3.

$$PMV = 0.3134 \times SET^{*2} - 7.41, \quad (R^2 = 0.96, P < 0.001) \quad (2)$$

$$AMV = 0.0327 \times SET^{*2} - 1.4552 \times SET^* + 16, \quad (R^2 = 0.94, P < 0.001) \quad (3)$$

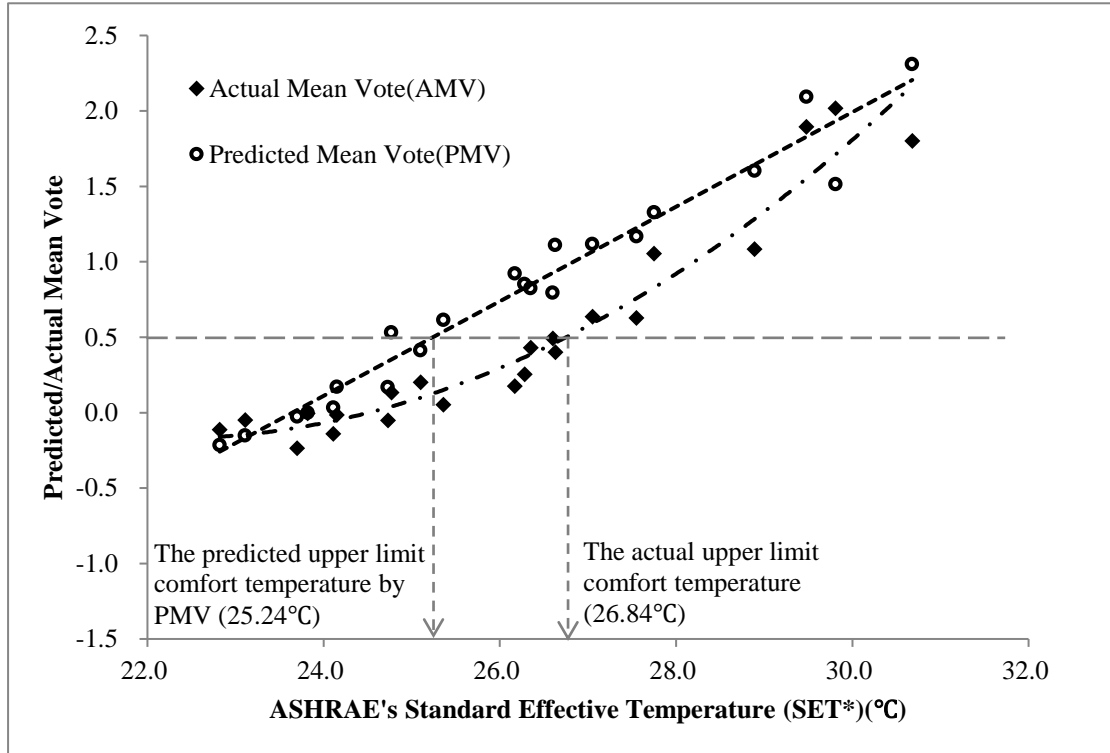


Figure 3. Thermal sensation votes (PMV and AMV) against ASHRAE Standard Effective Temperature (SET*) for all measured data.

From Figure 3 we can see that, at the thermal comfort upper limit point $PMV/AMV=0.5$, the related SET* temperatures are 25.24°C and 26.84°C respectively to the PMV and AMV estimations. Apparently, the PMV overestimates thermal sensation and leads to a lower SET* upper limit. The adverse effects will cause an overuse of energy for cooling in air-conditioning.

3.2 PMV and AMV

PMV predicts the actual thermal sensation well around the neutral thermal sensation point (when $PMV=0$) (see Figures 2, and 3). This finding endorses de Dear's claim that '*PMV appears to have been remarkably successful at predicting comfort temperatures in the HVAC buildings*'. However, from the figures, we can see that in the warm conditions (when $PMV > 0$), PMV overestimates actual thermal sensations. In order to rigorously investigate the agreement of the two indices (AMV and PMV), the Bland-Altman [31, 32] analysis method was applied. The values of the AMV and the PMV in each condition (marked as AMV_i and PMV_i) were regarded as a pair. The average value of each paired sample (AV_i), the value of the difference of each paired sample ($AMV-PMV$), the mean difference (\bar{d}) and the standard deviation of the

differences (s_d) were calculated by Equations 4, 5, 6, 7; as demonstrated in Figure 4.

$$AV_i = (PMV_i + AMV_i) / 2 \quad (4)$$

$$d_i = AMV_i - PMV_i \quad (5)$$

$$\bar{d} = \frac{1}{n} \sum_{i=1}^n d = 0.296 \quad (6)$$

$$s_d = \sqrt{\sum_{i=1}^n (d - \bar{d})^2 / (n - 1)} = 0.296 \quad (7)$$

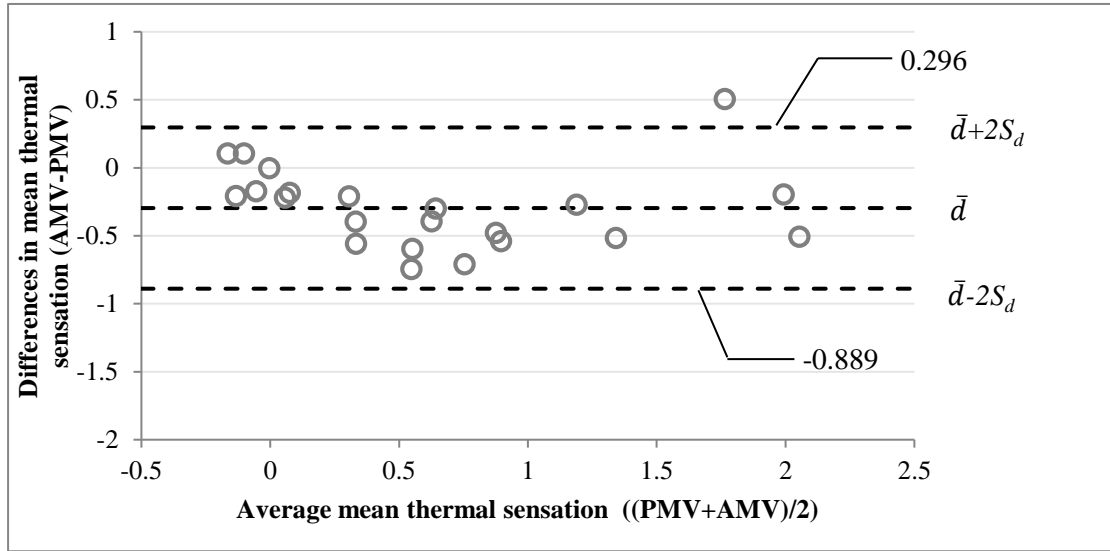


Figure 4. Differences of PMV and AMV against mean for AMV/PMV data

From Figure 4 we can see that the differences of the AMM and PMV are uniformly distributed around the mean difference (\bar{d}) and lie within the range $\bar{d} - 2s_d$ to $\bar{d} + 2s_d$. According to the Bland-Altman method, the ‘limits of agreement’ estimated by the values of $\bar{d} \pm 2s_d$ provides an interval within which 95% of the differences between AMV and PMV are expected to lie, this interval is defined using the Equations 8 and 9:

$$\bar{d} - 2s_d = 0.296 - 2 \times (-0.296) = 0.296 \quad (8)$$

$$\bar{d} + 2s_d = 0.296 + 2 \times (-0.296) = -0.889 \quad (9)$$

The value of the ‘limits of agreement’ indicates that the AMV is about 0.296 above the

PMV or 0.889 below the according to the ASHRAE thermal sensation scale. As described in Section 2.5, the PMV and AMV can be interchangeable only if the provided differences within the ‘limits of agreement’ are acceptable to professional knowledge. In the assessment of PMV performance, Humphreys *et al.* [18] argued that it would be necessary for the prediction to be within ± 0.1 scale unit. Considering that the prediction-bias of the group comfort votes were usually greater than this figure, he suggested that the PMV would need to correspond closely to the actual mean vote of the occupants at least within ± 0.25 scale unit, otherwise the bias of PMV was unacceptable. The ‘limits of agreement’ obtained by the Bland-Altman method cannot meet the lowest criteria suggested by Humphreys. Therefore, we can regard the AMV and PMV in this study as lacking in agreement and that there is a remarkable bias of PMV when applied in the well-controlled environment in the hot-humid region.

3.3 Skin Temperature

For each experiment condition bin, we calculated the mean value and standard deviation of subjects’ mean skin temperature (MST). Figure 5 illustrates the relationship between MST and SET*. In the figure, the predicted values of mean skin temperature were obtained using the two-node model proposed by Gagge [34]; and the measured mean skin temperatures were obtained from our experiment measurements. The results show that when SET* is above 25°C, the differences between the measured and predicted values are statistically insignificant ($P > 0.05$, one sample T-test), which means the measured value of the mean skin temperature matches well with the predicted value. However, for the experiment conditions where SET* lies between 23-25°C (marked within the rectangle with dashed lines), the measured values are nearly all significantly lower than the prediction ($P < 0.05$, one sample T-test), the biggest value of difference is about 0.5°C.

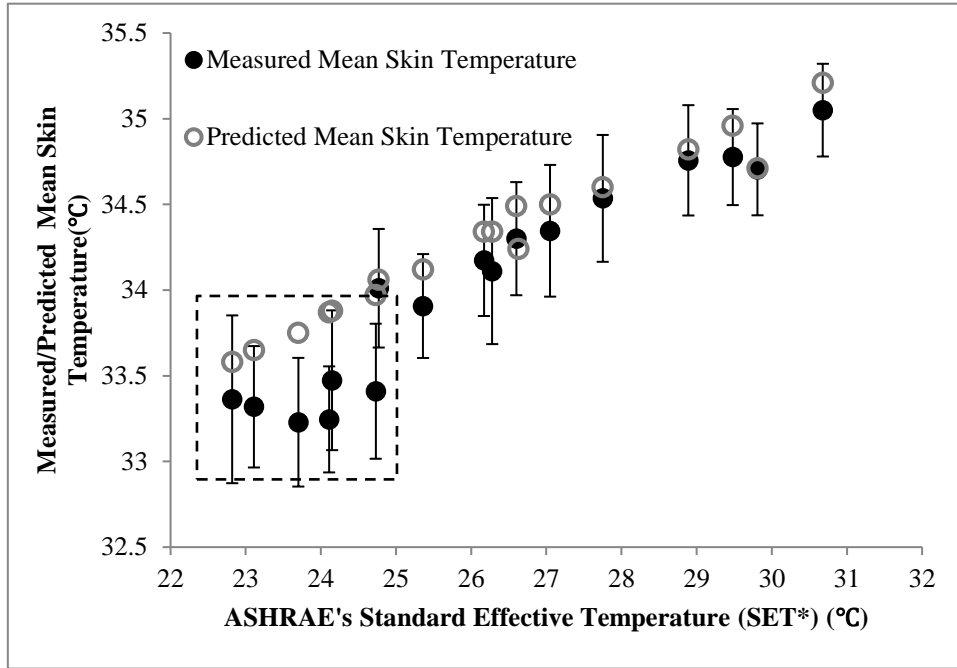


Figure 5. Measured and predicted mean skin temperature related with SET*.

The Boltzmann fit was used for regression analysis to work out the relation between the AMV and the MST as demonstrated in Figure 6 where each black square represents the average value of 20 observations in a bin. The fitted curve (the dash line) could be referred as the 'thermal sensibility curve for skin' in the hot-humid region. Equation 10 is the regression equation used.

$$AMV = 3.6 - 3.72 / \{1 + \exp[(MST - 34.8) / 0.3]\} \quad (R^2=0.87, P<0.001) \quad (10)$$

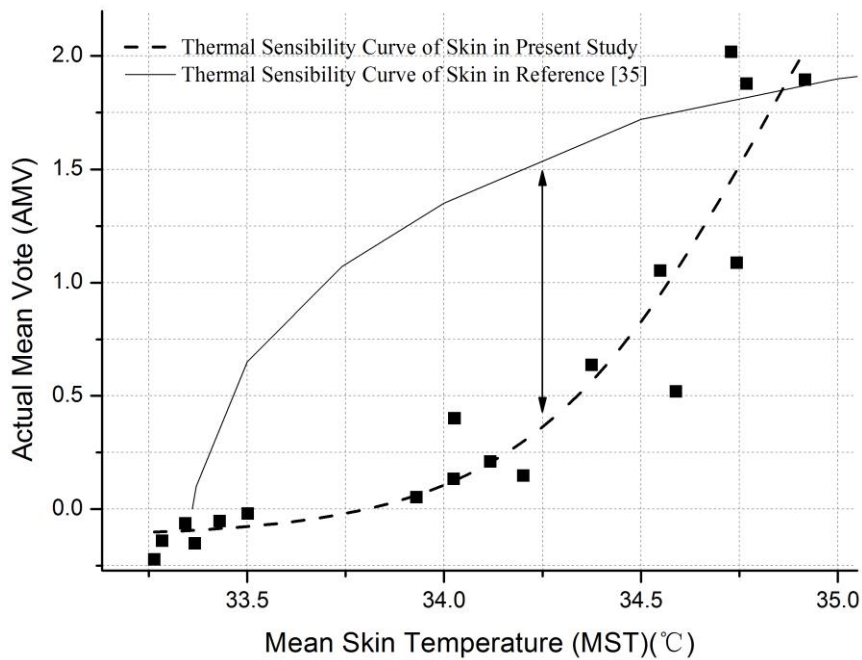


Figure 6. Subjects' thermal sensibility curves to skin temperature

In order to identify the thermal sensibility to skin temperature of subjects from different regions, the curve in our study was compared with the existing research outcome from Gagge *et al.* conducted in the U.S [35]. Gagge's thermal sensibility curve is presented in a solid line in Figure 6. From this figure we can see a significant discrepancy between the results of these two studies. There is no strong relation between actual mean vote and mean skin temperatures when MST is lower than 34°C as shown in our study (actual mean vote is less than 0.15 scale unit). In contrast, Gagge's results demonstrate a marked sensations of warmth appearing at the point where MST is lower than 34°C (actual mean vote is greater than 1 scale unit).

4. Discussion

The open literatures provide overwhelming evidence supporting the identification of human thermal adaptation from field studies rather than from climate chamber laboratory experiments [6]. To study the human adaptation in central controlled HVAC environments, de Dear and Brager [6] and Humphreys and Nicol [18] analyzed data from the HVAC building field study from the RP-884 database. Although field studies are best for assessing the potential impact of behavioral and psychological adaptations

as they occur in the real environment, it is hard to identify the significance of the contribution from each adaptation category. Only the joint effect can be assumed in the field studies. On the contrary, the climate chamber study provides the opportunity to rule out some variables regarded as the causation of the PMV-bias in real centralized HVAC buildings. We specifically focused on key variables by fixing the others and identifying the mechanism of adaptation.

4.1 Experiment conditions

The experiment conditions in our study are almost the same as those used by Fanger in the 1970s except for two aspects: i) the subject exposure time and ii) regional climatic experience of the subjects in the experiments.

Subject exposure time

The exposure time in Fanger's experiments was 3 hours in order to obtain a steady state for the human body; whilst the exposure time in the our study is 1.5 hours. In our experiments, the mean skin temperature achieved steady-state when the exposure time is 30 minutes. Therefore, the 1.5 hour exposure time is adequate for the human body to achieve a physiological steady state. It is thus reasonable to assume no essential difference between the two experiments in terms of the exposure time.

Subject climatic experience

Fanger's PMV model is based on the experiments involving subjects from America and Europe [5]. The targeted subject groups were not from a single, specific, climate region. In our case, all the subjects had a long-term acclimatised thermal history of hot-humid experience before they participated in the experiment.

To summarise, the difference between our experiments and Fanger's is that our targeted group of subjects are a unique group in which all subjects have a long-term acclimatised thermal history of hot-humid experience.

4.2 Identification of the causes of the bias of PMV

In our climate chamber experiments, both physical environments and human activity were strictly controlled, and each subject was clothed uniformly. There were no behavioural adaptation opportunities for subjects in the experiment. As the behavioural

adaptation factor has been ruled out, we will next analyse another two categories of adaptation: physiological and psychological.

4.3 Physiological adaptation

By definition, physiological adaptation includes changes in the physiological responses that result from exposure to thermal environmental factors and which lead to a gradual diminution of the strain induced by such exposure [36]. Acclimatisation is a subcategory of physiological adaptation which is closely related to the occupant's thermal living environment and thermal experience history [6].

According to the knowledge of thermogulation theory and heat transfer theory, any thermal physiological response will result in the change of temperature of human body. By analysing the research in the thermogulation model of human body [34, 37], we found the skin temperature was the most sensitive indicator to the physiological response. Taking the simplified model of Gagge as an example [34], showing in the Equation 11 and 12, the physiological responses of sweating, vasoconstriction, vasodilation, metabolic rate and shivering will directly or indirectly affect the value of skin temperature. Moreover, the skin temperature was often used to represent the results of the physiological responses in the thermogulation model studies [38-40]. Therefore, the skin temperature is chose as an indicator for the study of physiological adaptation in this paper. If there's any physiological adaptation that lead to any changes in the physiological responses, then the skin temperature should be changed as well.

$$m_s c_s \frac{T_s}{dt} / A = (K + c_b V_b)(T_c - T_s) - C - R - E_{dif} - E_{rsw} \quad (11)$$

$$m_c c_c \frac{T_c}{dt} / A = M + M_{shi} - E_{res} - w - (K + c_b V_b)(T_c - T_s) \quad (12)$$

From Figure 5, we can see that when SET* is between 23 and 25°C and MST lies in the range of 33-34°C the measured mean skin temperature was significantly lower than the predicted value by almost 0.5°C using Gagge's prediction model which was based on the group of people who are not from this region. The changes in skin temperature caused by physiological response decrease the stimulus of the thermal environment to the human body, and consequently lead to thermal sensation reports becoming more towards neutral. The phenomenon has been regarded as a physiological

adaptation of the human body. As illustrated in Section 3.2 and shown in Figure 6, the variation of mean skin temperature contributes a small (0.15) scale unit to the actual thermal sensation vote within the MST range of 33-34°C (around neutral point). This implies that the significant physiological adaptation does exist but only over a small range of indoor temperature which could lower the skin temperature, but the contribution to the thermal comfort vote is not significant.

4.4 Psychological adaptation

The effect of physiological factors on the PMV has been regarded as insignificant based on the actual thermal sensation, thus psychological adaptation turns into the most significant explanation. The psychological dimension of thermal adaptation is defined as “an altered perception of, and reaction to, sensory information due to past experience and expectations” [6]. The skin temperature can typically represent the major information of such thermal sensory system this is because plenty of the thermoreceptors of human body are distributed in the skin [41]. Thus subjects’ thermal sensibility to skin temperature reasonably reveals this “perception of, and reaction to, sensory information”. According to the results in Figure 6, the thermal sensibility curve to the skin of the subjects in the hot-humid region significantly differs from the curve of Gagge’s data. In principle, when subjects have the same MST, they should have the same sensory information. However, the intensity of warm sensations of subjects with a hot-humid climate background in our study is weaker than that of the subjects from Gagge’s study (as the arrow shown in Figure 6). This moderated thermal sensibility to skin temperature indicates that subjects’ thermal perception has been altered, i.e. psychological adaptations have been generated. The differences between the values of the two sensibility curves generated from two different groups of subjects from different climates indicate a quantitative value for the magnitude of psychological adaptation. It is therefore revealed that psychological adaptation creates a drop in the thermal sensation vote around the boundary of the comfort zone, which effectively accounts for the overestimation of PMV in a warm environment. It can be concluded that psychological adaptation does exist in the well-controlled environment and that it is the primary factor that makes the thermal sensation neutralised and the comfort zone wider.

Psychological adaptation is usually recognized to play a role in terms of habituation and expectation. Previous studies in psychological adaptation focusing on the role of

personal control indicated that psychological adaptation is a key factor influencing occupant expectations [42] and that it has important implications in naturally-ventilated vs. centrally-air-conditioned buildings [36]. Such expectations were usually embodied in the change of preferred temperature in the naturally ventilated buildings [37]. However, in our climate chamber study, personal control was restricted and the expectation effect was limited. Therefore, the psychological adaptation shown in the well-controlled environment is distinguished from that in a naturally-ventilated environment and should result from the effect of habituation, which is quite related to people's thermal experience history. It is inferred that the subjects with a thermal experience history of a hot-humid climate have generated a certain kind of habituation due to the long time spent living in such a region. Such habituation alters the subjects' thermal sensibility to skin temperature and results in the neutralization of the intensity of thermal sensation.

4.5 Application of adaptive principle in thermal engineering

The discussion above demonstrates the disagreement between the PMV and the AMV in a well-controlled environment in the hot-humid climate region. This indicates the discrepancies between the PMV and AMV in a well-controlled environment in the hot-humid region. As illustrated in Section 3.1, the PMV overestimates the actual thermal sensation thus leading to an unnecessarily lower temperature setting in an air-conditioned building with a consequent wastage of energy for cooling. Therefore, the PMV index needs to be adjusted when it is applied for thermal comfort assessment in the hot-humid region. A polynomial regression of the PMV and AMV has been produced based on the experimental data collected in this study. The adaptive thermal sensation vote PMV_a is proposed as Equation 13:

$$PMV_a = 0.22PMV^2 + 0.45PMV - 0.1 \quad (13)$$

The correlation is significant ($R^2=0.85$, $P<0.001$). Figure 7 shows the polynomial regression of the PMV and PMV_a .

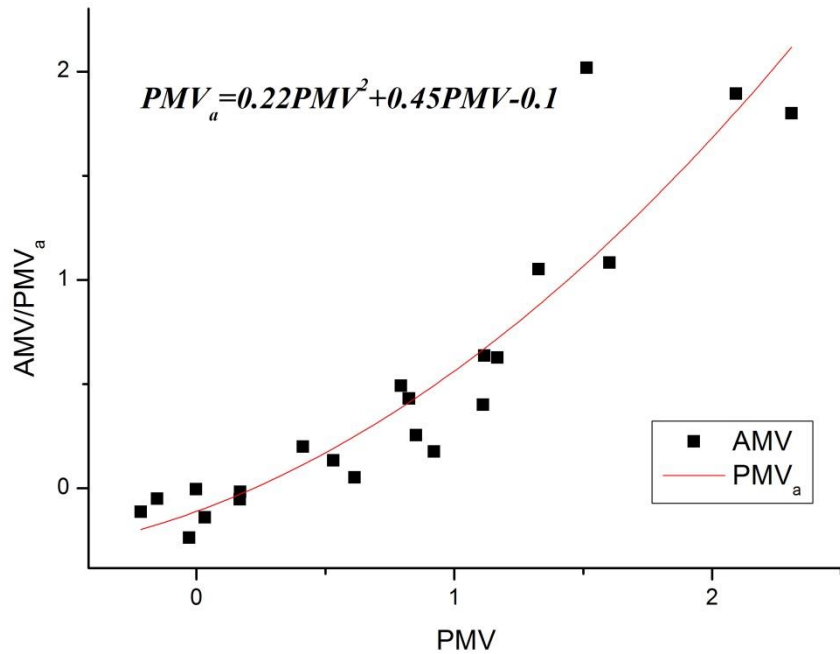


Figure 7. PMV_a and AMV against PMV

The air-conditioning setting point significantly affects energy consumption and occupants' thermal sensation. Adaptive thermal comfort theory has been widely accepted in the naturally ventilated/free running buildings. However, little studies have been done in a well-controlled; air-conditioning system equipped environment. This fundamental research studies the impact of habituation factor on human thermal sensation and moderates the traditional thermal comfort model with a new index PMV_a in the hot-humid region in China. The moderated PMV_a index will provide a new acceptable temperature range for an air-conditioning system design and operation. Furthermore, the adaptive thermal comfort principle will fully support the engineering solution of a hybrid system (passive and mechanical active) design and dynamic operation strategies of the environmental system.

5. CONCLUSIONS

This paper presents an investigation on thermal sensation and adaptation in a well-controlled climate chamber for people who have a hot-humid climate thermal experience history. It is revealed that the 'limit of agreement' between the PMV and AMV is in the range of -0.889 and 0.296 by using the Bland-Altman agreement

assessment method. The result indicates that the PMV and AMV are lacking in agreement; therefore in principle, the PMV could be amended in its application in air-conditioned environments in this region. The PMV predicts neutral comfort temperature well (when $PMV=0$), however, it overestimates thermal sensation in a well-controlled environment in the warm condition (when $PMV > 0$).

The bias of the PMV from the AMV can be regarded as the thermal adaptation generated by the past thermal experience of a long time spent living in a specific region. This thermal adaptation can be regarded as a joint effect of the non-significant factor of acclimatisation due to the physiological response and the significant habituation due to psychological adaptation. However, the psychological adaptation contributes the most to the thermal sensation vote. The psychological adaptation neutralizes people's thermal sensation by means of reducing the thermal sensibility of the skin. The contribution of habituation to the actual thermal sensation of two groups of people from different regions can be quantified by calculating the differences between the thermal sensibility curves to the skin temperature.

A revised PMV index, named as PMV_a , has been derived as an empirical equation:

$$PMV_a = 0.22PMV^2 + 0.45PMV - 0.1$$

which is suitable for application in an air-conditioned building in the hot-humid region in China. Therefore, the ASHRAE Standard thermal comfort temperature SET* upper limit could be adjusted by a 1.6°C increase from 25.24°C to 26.84°C. This adjustment will be instructive to the creation of indoor thermal environment and significantly contribute to energy efficiency in buildings.

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