

Interaction of the convective energy cycle and large-scale dynamics

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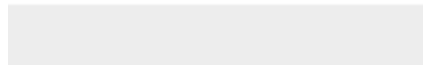
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Abstract:	The importance of the convective life cycle in tropical large-scale dynamics has long been emphasized, but without explicit analysis. The present work provides it by coupling the convective energy cycle under the framework of Arakawa and Schubert's (1974) convection parameterization with a shallow-water analogue atmosphere. The square frequency of linear convectively--coupled waves is given by a squared sum of the dry gravity-wave and the convective energy-cycle frequencies, hortening the period of the convective cycle through the large-scale coupling. In a weakly nonlinear regime, the system follows an equation analogous to the Kortweg-de Vries equation, which exhibits a solitary--wave solution, with behavior reminiscent of observed tropical westerly--wind bursts.
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1 **Interaction of the Convective Energy Cycle and Large-Scale Dynamics**

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6 ABSTRACT: The importance of the convective life cycle in tropical large-scale dynamics has
7 long been emphasized, but without explicit analysis. The present work provides it by coupling
8 the convective energy cycle under the framework of Arakawa and Schubert's (1974) convection
9 parameterization with a shallow-water analogue atmosphere. The square frequency of linear
10 convectively-coupled waves is given by a squared sum of the dry gravity-wave and the convective
11 energy-cycle frequencies, shortening the period of the convective cycle through the large-scale
12 coupling. In a weakly nonlinear regime, the system follows an equation analogous to the Kortweg-
13 de Vries equation, which exhibits a solitary-wave solution, with behavior reminiscent of observed
14 tropical westerly-wind bursts.

16 **Significance Statement:** The present work suggests that a nonlinear description of a large-scale
17 tropical system with an explicit convective life cycle may provide a simple model of tropical
18 westerly-wind bursts. At the same time, an important lesson to learn is that, if the focus of
19 a study is on the global scale of the atmosphere, it is wise not to try to include a convective
20 life cycle explicitly into the model. Such a configuration will simply be dominated by the short
21 convective-scale variabilities, that one would wish to filter out.

22 1. Introduction

23 It is commonly accepted that tropical atmospheric dynamics is essentially described by the
24 interactions between large-scale equatorial waves and small-scale convection: *cf.*, critical reviews
25 in introductions of Yano and Tribbia (2017), Yano and Wedi (2021), and further references therein.
26 A standard approach has been to introduce parameterized convection to the large-scale dynamics
27 under a general framework of convective quasi-equilibrium (*cf.*, Yano and Plant 2012a), which
28 assumes that small-scale convection is in equilibrium with the large-scale dynamics in a certain
29 manner. This general conceptual framework can cover a wide range of formulations, including
30 the original one by Arakawa and Schubert (1974), but also a more straightforward assumption
31 of convective neutrality of the large scale, originally suggested by Betts (1986), observationally
32 supported by Xu and Emanuel (1989), and applied to theoretical studies by Emanuel (1987) and
33 Neelin *et al.* (1987). More classical approaches of wave-CISK (Hayashi 1970, Lindzen 1974) can
34 also be included in this category in the present context. All of these approaches have in common
35 that they *do not* introduce an explicit process characterized by a convective time scale.

36 At the same time, there has been a persistent feeling in the tropical community that a finite time
37 scale for the life cycle of small-scale convection plays a critical role in the tropical large-scale
38 dynamics. This feeling may be, for example, reflected upon through brief, albeit rather obscure
39 discussions on the convective life cycle leading to his Eqs. (2.2) and (3.6) in Kuo (1974), the
40 emphasis on mesoscale processes for convection parameterizations in the review by Houze and
41 Betts (1981), and probably most succinctly summarized by an argument of activation-control by
42 Mapes (1997).

43 The most straightforward way to include a convective time scale within a parameterization is
44 to introduce it as a finite-time adjustment process towards an equilibrium. A parameterization by
45 Betts (1986) follows this approach, although his main focus in the formulation is in defining an
46 equilibrium profile. Neelin and Yu (1994) and Yu and Neelin (1994) introduced this finite-time
47 convective adjustment in the context of large-scale dynamic studies. Similar approaches are adopted
48 by *e.g.*, Frierson *et al.* (2004), Stechmann and Majda (2006), Bouchut *et al.* (2009), Lambaerts
49 *et al.* (2011). However, these convective adjustment approaches are still short of introducing a
50 life-cycle of convection: adjustment only describes a monotonic approach towards an equilibrium,
51 without going through anything like a cycle. A simple model for the convective life cycle was
52 introduced by Yano and Plant (2012b).

53 Yano and Plant (2012b) showed that a basic behavior of atmospheric deep convection, especially
54 its tendency for following a cycle of discharge and recharge (*cf.*, Blade and Hartmann 1993),
55 can be described by an energy cycle, as originally introduced by Arakawa and Schubert (1974)
56 as their Eqs. (132) and (140), but by adding simple closures to this system (*cf.*, Eq. 2.5 below).
57 A key simplification in the formulation of Yano and Plant (2012b) is to consider only a single,
58 deep convection mode so that the integral kernel, defined by Eqs. (B36) and (B37) in Arakawa and
59 Schubert (1974), reduces to a single scalar parameter.

60 The purpose of the present study is to couple this convective energy cycle system with a simple
61 large-scale dynamics described by a shallow-water analogue, and to present its basic behavior.
62 The most fascinating finding from this study is the existence of a solitary wave solution under
63 weak nonlinearity, whose behavior is reminiscent of observed tropical westerly-wind bursts (*cf.*,
64 Hartten 1996, Yano *et al.* 2004).

65 The convective energy-cycle system introduced by Yano and Plant (2012b) is reviewed in the next
66 section. As a first step for investigating the coupled dynamics of this system, we adopt a simple
67 horizontally one-dimensional shallow-water analogue for the large-scale dynamics, as introduced
68 in Sec. 3. A complete formulation of the system is presented in Sec. 4 in a nondimensional form.
69 The derived system is analyzed over Secs. 5–7 in three steps: steady solutions (Sec. 5), linear
70 waves (Sec. 6), and a weakly nonlinear analysis (Sec. 7). The paper is concluded by Sec. 9 after
71 further discussions in Sec. 8.

72 **2. Convective Energy-Cycle System (Dimensional)**

73 Following Yano and Plant (2012b), the convective energy-cycle system is given by:

$$\frac{dK}{dt} = AM_B - D, \quad (2.1a)$$

$$\frac{dA}{dt} = -\gamma M_B + F \quad (2.1b)$$

74 with the convective kinetic energy, K , and the cloud work function, A , as prognostic variables.

75 These are defined by

$$K = \int_{z_B}^{z_T} \sigma \frac{\rho}{2} w_c^2 dz, \quad (2.2a)$$

$$A = \int_{z_B}^{z_T} \eta b dz. \quad (2.2b)$$

76 Here, notably, σ is the fractional area occupied by convection, η is a normalized vertical profile
 77 of convective mass flux, and M_B is the convective mass flux at the convection base. The other
 78 variables introduced in Eqs. (2.2a, b) are: ρ the air density, w_c the convective vertical velocity, z
 79 the vertical coordinate, and b the buoyancy.

80 Arakawa and Schubert (1974) assumed an entraining plume profile in defining the cloud work
 81 function, A . In this case, the profile, η , is normalized by the value at the convective base. However,
 82 Yano *et al.* (2005) show that the concept of the cloud work function can be applied to any vertical
 83 convective profile, η , as a measure of the potential energy convertibility (PEC), as seen on the first
 84 term in the right-hand of Eq. (2.1a). Note further that if we set $\eta = 1$, the cloud work function
 85 (PEC) reduces to a form of convective available potential energy (CAPE). It fully reduces to CAPE
 86 if the buoyancy, b , is defined as that of a lifting parcel. However, the definition of the buoyancy
 87 is kept open in Eq. (2.2b): for example, it could be taken as the buoyancy as defined in explicit
 88 convection simulations, averaged over the convective area.

89 We assume that the convective damping, D , is expressed by a Rayleigh damping:

$$D = \frac{K}{\tau_D} \quad (2.2c)$$

90 with the damping time scale, $\tau_D \sim 10^3$ sec. γ measures the efficiency with which convection
 91 consumes the cloud work function (PEC), A , with time, corresponding to the kernel, \mathcal{K} , introduced
 92 by Arakawa and Schubert (1974), but reducing it to a scalar by only considering a single convective
 93 mode here.

94 The large-scale forcing, F , was taken to be a prescribed constant in Yano and Plant (2012b) in
 95 order to consider the convection dynamics in a stand alone manner. For the present purpose of
 96 considering a coupling of this energy-cycle system with the large-scale dynamics, the large-scale
 97 forcing must evolve following the evolution of the large-scale state. Thus, we define it by

$$F \simeq \int_{z_B}^{z_T} \frac{g\eta}{\bar{T}} \left(\bar{w} \frac{\partial \bar{\theta}}{\partial z} - Q_R \right) dz, \quad (2.2d)$$

98 where g is the acceleration due to gravity, \bar{T} the large-scale temperature, \bar{w} the large-scale velocity,
 99 $\bar{\theta}$ the large-scale potential temperature, and Q_R the radiative heating rate. It is important to note that
 100 we neglect a contribution of boundary-layer processes to the large-scale forcing in the definition
 101 (2.2d). This simplification is consistent with that which Arakawa and Schubert (1974) adopted
 102 in their quasi-equilibrium diagnosis, as well as the observationally-proposed approximation of
 103 parcel-environment quasi-equilibrium (Zhang 2002, 2003, Donner and Phillips 2003).

104 Finally, the vertical integrals in Eqs. (2.2a, b, d) are, in principle, performed from the convection
 105 base, z_B , to its top, z_T . However, for the sake of simplifying the coupling with the large-scale
 106 dynamics, we re-set them to be the surface, $z_B = 0$, and the top of the atmosphere, z_T . By adopting
 107 an equivalent vertical coordinate in the large-scale dynamics (*cf.*, Sec. 3), z_T , can easily be
 108 re-interpreted as the top of the troposphere.

109 For achieving the simplest possible coupling, we still assume that the radiative heating rate, Q_R ,
 110 is prescribed, but modify the first term in the definition (2.2d) above, by following the evolution of
 111 the large-scale vertical velocity, \bar{w} . We assume a normalized vertical profile of the vertical velocity,
 112 \bar{w} , to be W so that

$$\bar{w} = \tilde{w}(x, t) W(z). \quad (2.3a)$$

113 Here, $\tilde{w}(x, t)$ designates the horizontal dependence of the large-scale vertical velocity, and x is the
 114 only horizontal coordinate. Throughout the paper, vertical profiles are designated by upper-case
 115 letters, and keep in mind that all of the vertical profiles are defined to be nondimensional, and also

116 normalized to $O(1)$. Furthermore, the tilde sign is added to distinguish the horizontal components
 117 until the end of Sec. 3.

118 As a result, the large-scale forcing may be re-written as:

$$F = \mu \tilde{w} + F_R, \quad (2.3b)$$

119 where

$$\begin{aligned} \mu &= \int_{z_B}^{z_T} \frac{g\eta}{\bar{T}} W \frac{d\bar{\theta}}{dz} dz \\ &\sim \frac{gH}{T_0} \frac{d\bar{\theta}}{dz} \sim \frac{10 \text{ m/s}^2 \times 30 \text{ K}}{300 \text{ K}} \\ &\sim 1 \text{ m/s}^2 \end{aligned} \quad (2.4a)$$

120 measures the efficiency with which large-scale ascent generates the cloud work function (PEC), A .
 121 The second term in Eq. (2.3b),

$$F_R = - \int_{z_B}^{z_T} \frac{g\eta}{\bar{T}} Q_R dz, \quad (2.4b)$$

122 measures the rate at which the cloud work function (PEC) is generated by radiative cooling.

123 Finally, for closing the system, as in Yano and Plant (2012b), we assume a relation

$$K = \beta M_B, \quad (2.5)$$

124 where β is a constant estimated to be $\beta \sim 10^4 \text{ m}^2/\text{s}$.

125 3. Large-Scale System

126 As a first step in constructing a large-scale system to be coupled with the convective energy cycle
 127 system introduced in the last section, we consider the large-scale heat equation in Sec. 3.a, because
 128 it is the key equation to achieve a coupling of the two scales. The formulation is completed more
 129 formally by introducing the normal mode decomposition of the linear primitive equation system in
 130 Sec. 3.b. The presentation is rather backwards, because the first subsection has to quote some of
 131 the results to be obtained in the following subsection. Nevertheless, we present in this order for the
 132 sake of making the physical motivations clear before a more complete mathematical formulation

133 is provided. The system is assumed linear throughout this section. Nonlinear advection terms will
 134 be considered later in Sec. 4.e.

135 *a. Large-Scale Heat Equation*

136 A major feedback of convection to the large-scale state is found in the heat equation, which may
 137 be written as

$$\frac{\partial \theta}{\partial t} + w \frac{d\bar{\theta}}{dz} = Q_c + Q_R. \quad (3.1)$$

138 Here, Q_c is the convective heating rate, approximately given by:

$$Q_c = \sigma w_c \frac{d\bar{\theta}}{dz} \quad (3.2)$$

139 neglecting the effect of detrainment for simplicity (*cf.*, Yano and Plant, 2020). Recall that Q_R is
 140 the radiative heating.

141 Because the convective dynamics is described in terms of a single vertical mode, it is appropriate
 142 to reduce the large-scale dynamics similarly. For this reason, we have already assumed only a
 143 single vertical mode for the large-scale dynamics by writing the vertical velocity in the form of
 144 Eq. (2.3a) in Sec. 2, and equivalently, the potential temperature is represented by:

$$\theta = \tilde{\theta}(x, t) \Theta(z). \quad (3.3)$$

145 Here, Θ is a nondimensional, normalized vertical profile and $\tilde{\theta}$ describes the horizontal dependence.
 146 We also set

$$\sigma w_c = \frac{\eta}{\rho_0} M_B = \eta \tilde{w}_c,$$

147 where ρ_0 is the surface density.

148 As a standard procedure for projecting an equation onto a given vertical mode, we multiply
 149 Eq. (3.1) by Θ , and integrate it vertically. As a result, we obtain

$$\frac{\partial \tilde{\theta}}{\partial t} + \frac{\theta^*}{z_T} \tilde{w} = \hat{\eta} \tilde{w}_c - \hat{Q}_R^* w_R, \quad (3.4)$$

150 where

$$\frac{\theta^*}{z_T} = \left\langle W \Theta \frac{d\bar{\theta}}{dz} \right\rangle = \frac{\theta_0 h_E}{z_T^2}, \quad (3.5a)$$

$$\hat{\eta} = \left\langle \eta \Theta \frac{d\bar{\theta}}{dz} \right\rangle, \quad (3.5b)$$

$$\hat{Q}_R^* = -\langle \Theta Q_R \rangle. \quad (3.5c)$$

151 Here, we define the angled brackets as an integral operator

$$\langle * \rangle = \frac{1}{z_T} \int_0^{z_T} * dz,$$

152 setting $z_B = 0$ in previous vertical integrals, as already discussed. We have also assumed that Θ is
 153 normalized by

$$\langle \Theta^2 \rangle = 1.$$

154 We further introduce θ^* as a characteristic scale for θ . An alternative representation is also given
 155 in Eq. (3.5a) in terms of a reference value of potential temperature, θ_0 and an equivalent depth, h_E :
 156 this form will prove convenient later.

157 It will be shown in next subsection that the vertical–wind profile, W , is related to the potential–
 158 temperature profile, Θ , by:

$$W = \frac{\theta^*}{z_T} \left(\frac{d\bar{\theta}}{dz} \right)^{-1} \Theta. \quad (3.5d)$$

159 from Eq. (3.11b) to be derived below.

160 Additionally, the nondimensional radiative vertical velocity, w_R , has been introduced in Eq. (3.4),
 161 in order to represent a possible horizontal distribution of radiation. This study assumes the radiation
 162 to be horizontally homogeneous and thus we will simply set it to unity in the following, but explicitly
 163 re-introduce it whenever important to indicate the role of radiation in a given equation.

164 With the final goal of reducing the system to a shallow-water analogue in mind, it is convenient
 165 to replace the potential temperature, $\tilde{\theta}$, in the heat equation (3.4) by the height field, \tilde{h} . These two
 166 variables are linked together through hydrostatic balance, as will be obtained in Eq. (3.12b) below:

$$\tilde{h} = -\frac{h_E}{\theta^*} \tilde{\theta} = -\frac{z_T}{\theta_0} \tilde{\theta}. \quad (3.6)$$

167 As a result, the heat equation reduces to:

$$\frac{\partial \tilde{h}}{\partial t} - \hat{S}(\tilde{w} - \alpha \tilde{w}_c) = \hat{Q}_R. \quad (3.7)$$

168 Here, the introduced nondimensional parameters are estimated as:

$$\hat{S} = \frac{h_E}{z_T} \sim 10^{-2}, \quad (3.8a)$$

$$\alpha = \frac{z_T}{\theta^*} \hat{\eta} = \frac{z_T^2}{\theta_0 h_E} \hat{\eta} \sim 1, \quad (3.8b)$$

$$\hat{Q}_R = \frac{h_E}{\theta^*} \hat{Q}_R^* = \frac{z_T}{\theta_0} \hat{Q}_R^*. \quad (3.8c)$$

169 Recall that $\hat{\eta}$ has already been defined by Eq. (3.5b). The orders of magnitude estimates in (3.8a,
170 b) are based on $h_E \sim 10^2$ m, $z_T \sim 10$ km, $\theta_0 \simeq 300$ K, and $\theta^* \sim 3$ K.

171 *b. Normal–Mode Decomposition of the Linear Primitive Equation System*

172 A thermodynamic formulation for a shallow-water analogue atmosphere has been introduced in
173 the last subsection, in which the large–scale heat equation reduces to a height equation for shallow
174 water. To complete the construction of a shallow–water analogue of the tropical atmosphere large-
175 scale dynamics, we now consider a full, linear primitive equation system to see how the vertical
176 profiles of the variables may be defined consistently. These profiles are usually called normal
177 modes (*cf.*, Kasahara and Puri 1981).

178 We consider a linear horizontally one-dimensional system with the Boussinesq approximation:

$$\frac{\partial u}{\partial t} = -\frac{\partial \phi}{\partial x}, \quad (3.9a)$$

$$\frac{\partial \phi}{\partial z} = g \frac{\theta}{\theta_0}, \quad (3.9b)$$

$$\frac{\partial \theta}{\partial t} + w \frac{d\bar{\theta}}{dz} = Q, \quad (3.9c)$$

$$\frac{\partial u}{\partial x} + \frac{\partial w}{\partial z} = 0. \quad (3.9d)$$

179 Here, θ_0 is a constant reference potential temperature, u is the horizontal velocity, and ϕ is the
180 geopotential. The total diabatic heating has been set to $Q = Q_c + Q_R$ as in the last subsection.

181 To apply the above system to a realistic atmosphere, the system is best re-interpreted as a
 182 consequence of transforming the pressure coordinate, p , into an equivalent geometrical coordinate,
 183 z , by the relation $dp = -\rho_0 g dz$ with ρ_0 a reference density, but with a minor modification to the
 184 hydrostatic balance (3.9b) of multiplying by an additional factor, $\rho_0 \theta_0 / \rho \bar{\theta}$ on the right-hand side.
 185 Keep in mind that all of the vertical integrals considered in the convective energy cycle formulation
 186 must also be re-interpreted accordingly.

187 We introduce a separation of variables by Eqs. (2.3a) and (3.3), as well as:

$$u = \Phi \tilde{u}, \quad \phi = \Phi \tilde{\phi}, \quad Q = \Theta \tilde{Q}. \quad (3.10a, b)$$

188 By substituting Eqs. (2.3a), (3.3), and (3.10a, b) into Eqs. (3.9a, b, c, d), we find that the vertical
 189 profiles must mutually satisfy the relations:

$$z_T \frac{d\Phi}{dz} = -\Theta, \quad (3.11a)$$

$$\Theta = \frac{z_T}{\theta^*} \frac{d\bar{\theta}}{dz} W, \quad (3.11b)$$

$$\Phi = z_T \frac{dW}{dz}. \quad (3.11c)$$

190 The two scales, z_T and θ^* , have been introduced so that all the vertical profiles consistently remain
 191 nondimensional, and also of the order unity.

192 By further substituting (3.11a, c) into (3.11b), we find:

$$\left[\frac{d^2}{dz^2} + \frac{1}{z_T} \left(\frac{1}{\theta^*} \frac{d\bar{\theta}}{dz} \right) \right] W = 0.$$

193 Here, $z_T \theta^*$ constitutes an eigenvalue in this equation. A more commonly accepted form is obtained
 194 by re-writing the above into:

$$\left[\frac{d^2}{dz^2} + \frac{1}{h_E} \left(\frac{1}{\theta_0} \frac{d\bar{\theta}}{dz} \right) \right] W = 0$$

195 with the equivalent depth,

$$h_E = \frac{\theta^*}{\theta_0} z_T,$$

196 constituting the standard engivenvalue of this problem (cf. Eq. 3.5a). It can be seen that the
 197 equivalent depth is the scaled-down version of the vertical scale by the relative fluctuation of the
 198 buoyancy with respect to the reference state.

199 Consequently, the equations for the horizontal components are given by:

$$\frac{\partial \tilde{u}}{\partial t} = -\frac{\partial \tilde{\phi}}{\partial x}, \quad (3.12a)$$

$$\tilde{\phi} = -\frac{gh}{\theta_0} \tilde{\theta} = -\frac{gh_E}{\theta^*} \tilde{\theta}, \quad (3.12b)$$

$$\frac{\partial \tilde{\theta}}{\partial t} + \frac{\theta^*}{z_T} \tilde{w} = \tilde{Q}, \quad (3.12c)$$

$$\frac{\partial \tilde{u}}{\partial x} + \frac{\tilde{w}}{z_T} = 0. \quad (3.12d)$$

200 By further setting, $\tilde{\phi} = g\tilde{h}$, re-writing Eq. (3.12c) in terms of \tilde{h} , we recover Eq. (3.7) already
 201 introduced. By eliminating the vertical velocity with the help of the mass continuity (3.12d), we
 202 find that the governing equation set for the horizontal components constitute an analogue of the
 203 shallow-water system with the equivalent depth, h_E playing the role of the depth.

204 4. Nondimensionalization

205 For ease of further analyses, we now nondimensionalize the system derived over Secs. 2–3.

206 a. Convective Energy-Cycle System

207 To nondimensionalize the convective energy cycle, we first note that the equilibrium state is
 208 given at the convective scale by:

$$A = A_0 \equiv \beta/\tau_D \sim 10\text{J/kg}, \quad (4.1a)$$

$$M_B = M_0 \equiv F_R/\gamma \sim 10^{-2}\text{kg/m}^2/\text{s}, \quad (4.1b)$$

209 where F_R is the radiative contribution to convective forcing. Estimates are based on the values of
 210 $\beta \sim 10^4 \text{ m}^2/\text{s}$, $\tau_D \sim 10^3 \text{ sec}$, $F_R \sim 10^{-2} \text{ m}^2/\text{s}^3$, $\gamma \sim 1 \text{ m}^4/\text{s}^2\text{kg}$ by following Yano and Plant (2012b).
 211 Setting, for now, the large-scale equilibrium to be simply quiescent, $\tilde{w} = \tilde{h} = 0$, we find that the

212 convection-base mass flux is further constrained to satisfy

$$M_B = \frac{\rho_0 \hat{Q}_R}{\alpha \hat{S}} \quad (4.1c)$$

213 from Eq. (3.7). Recall that \hat{Q}_R is a measure of the radiative cooling rate, as defined by Eq. (3.8c).

214 Obviously, this value must also agree with F_R/γ given by Eq. (4.1b).

215 We nondimensionalize the large-scale vertical velocity by:

$$\tilde{w} = w_0 \tilde{w}_*.$$

216 where the subscript * suggests a nondimensionalized horizontal dependence, and w_0 is the scale
 217 of the vertical velocity. Keep in mind that the subscript * will be tentative, and it will be removed
 218 as soon as the nondimensionalization is accomplished.

219 The appropriate time scale, τ_c , and vertical-velocity scale, w_0 for nondimensionalization are
 220 given by

$$\tau_c = (\beta/F_R)^{1/2} \sim 10^3 \text{ sec}, \quad (4.2a)$$

$$w_0 = F_R/\mu \sim 10^{-2} \text{ m/s}. \quad (4.2b)$$

221 The convective-scale variables are nondimensionalized into k_c and a by setting

$$M_B = M_0 k_c, \quad (4.3a)$$

$$A = \frac{\tau_D}{\tau_c} A_0 a, \quad (4.3b)$$

222 such that the resulting nondimensionalized equations are:

$$\frac{\partial k_c}{\partial t'} = a k_c - \frac{k_c}{\tau_D^*}, \quad (4.4a)$$

$$\frac{\partial a}{\partial t'} = -k_c + w + w_R, \quad (4.4b)$$

223 where the dependent variables are defined by:

- 224 • $k_c = w_c$: convective kinetic energy (or the convective mass flux)

225 • a : the cloud work function (which may conceptually be interpreted as a convective potential
 226 energy) .

227 $\tau_D^* = \tau_D/\tau_c$ is a nondimensional damping time scale, and $w_R (= 1)$ is a normalized radiative vertical
 228 velocity. In Eqs. (4.4a, b) the subscript * indicating nondimensional variables has already been
 229 removed.

230 As required, we use the following notations in an interchangeable manner

$$k_c = w_c \quad (4.5)$$

231 depending on the context. Note further that a prime sign is added to the nondimensional time, t' ,
 232 because a different nondimensionalization of time will be introduced for the large-scale dynamics
 233 in the next subsection.

234 *b. Large-Scale System*

235 We nondimensionalize the large-scale system by introducing the scales u_0 , h_0 , τ_L , and L , marking
 236 the nondimensional variables with the subscript * for now, thus, *e.g.*,

$$\frac{\partial}{\partial x} = \frac{1}{L} \frac{\partial}{\partial x_*}.$$

237 By substituting into Eqs. (3.12a, b, c), we find that convenient nondimensionalization scales are:

$$h_0 = h_E, \quad u_0 = c_g, \quad \tau_L = L/c_g, \quad (4.6a, b, c)$$

238 where $c_g = (gh_E)^{1/2}$ is the gravity-wave speed, and the characteristic horizontal scale, L , is left to
 239 be determined. We set $L = 3 \times 10^3$ km provisionally, for the purpose of some numerical estimates.

240 After removing the tilde signs, and removing the subscripts * from nondimensional variables,
 241 the resulting nondimensional set of equations are:

$$\frac{\partial u}{\partial t} = -\frac{\partial h}{\partial x}, \quad (4.7a)$$

$$\frac{\partial h}{\partial t} + \frac{\partial u}{\partial x} = -Q, \quad (4.7b)$$

$$w = -\hat{r}_L \frac{\partial u}{\partial x}. \quad (4.7c)$$

242 Here,

$$Q = \hat{\alpha}(w_c - w_R) = \hat{\alpha}w_c - \hat{Q}_R, \quad (4.8a)$$

$$\hat{r}_L = \frac{c_g z_T}{w_0 L} \sim 10, \quad (4.8b)$$

$$\hat{\alpha} = \alpha / \hat{r}_L, \quad (4.8c)$$

243 and \hat{r}_L may be considered an effective aspect ratio of the system. Alternatively, it can be interpreted
 244 as a ratio of two characteristic horizontal scales:

$$\hat{r}_L = L_D / L,$$

245 where

$$L_D = \frac{c_g z_T}{w_0} \sim 3 \times 10^4 \text{ km}.$$

246 Also keep in mind that the total depth of the shallow water is: $h_T = 1 + h$.

247 Recall from Eq. (3.7) that α controls the relative contributions of large-scale and convective-
 248 scale velocities to the stratification. The parameter, $\hat{\alpha}$ introduced by Eq. (4.8c) thus measures
 249 the efficiency of convection in modifying the stratification of the atmosphere, while $1 - \alpha$ may
 250 be considered a nondimensional measure of the effective stratification (or gross moist stability:
 251 Neelin and Held 1987). In particular, when $\alpha = 1$, the convective atmosphere is effectively
 252 neutrally stratified. Here, w_0 is a characteristic scale of the large-scale vertical velocity and, by
 253 nondimensionalization, the radiatively-driven vertical velocity is $w_R = 1$.

254 *c. Two Time Scales*

255 To couple together the two systems for convection and the large scale, we need to take care of
 256 the two different time scales adopted for the systems in nondimensionalization, τ_c (Eq. 4.2a) and
 257 $\tau_L = L/c_g$ (Eq. 4.6c). The ratio of the two is

$$\hat{r}_c = \tau_c/\tau_L \sim 10^{-2}. \quad (4.9c)$$

258 We will henceforth use τ_L for both systems for consistency. As a result, Eqs. (4.4a, b) are expressed
 259 as:

$$\hat{r}_c \frac{\partial k_c}{\partial t} = ak_c - \frac{k_c}{\tau_D^*}, \quad (4.9a)$$

$$\hat{r}_c \frac{\partial a}{\partial t} = -k_c + w + w_R. \quad (4.9b)$$

260 Note that for a large-scale horizontal scale of $L \simeq 30$ km, $\hat{r}_c \simeq 1$, and the two time scales match.

261 *d. Coupling Problem*

262 Through the considerations over the last subsections, we have arrived at a complete nondimen-
 263 sional set of equations given by (4.7a, b, c) and (4.9a, b). However, there remains one more issue
 264 to be addressed: the large-scale height, h , which is also related to the potential temperature, θ by
 265 Eq. (3.6), is effectively equivalent to the convective-scale cloud work function (PEC), a , because
 266 by neglecting contributions from the boundary layer, the buoyancy integral that defines a is deter-
 267 mined exclusively by contributions of the environmental potential temperature, also neglecting the
 268 virtual effect for the present purpose. Thus, a is nothing other than an alternative measure of the
 269 tropospheric potential temperature, in addition to h . Here, strictly speaking, we can still distinguish
 270 them by taking different vertical profiles in the definitions. However, retaining two measures of the
 271 potential temperature in a single-layer shallow-water analogue model would be rather redundant.
 272 Thus, we now reduce them to a single equation by establishing the equivalence of the two.

273 This is accomplished in the following manner, by introducing two additional constraints. By
 274 comparing between the right-hand side of Eq. (4.9b) and the definition (4.8a), we find that

$$\hat{r}_c \hat{\alpha} \frac{\partial a}{\partial t} - \hat{\alpha} w = -Q, \quad (4.10a)$$

275 also recalling that $k_c = w_c$. For comparison, the height equation (4.7b) is re-written with the help
 276 of Eq. (4.7c) as:

$$\frac{\partial h}{\partial t} - \frac{w}{\hat{r}_L} = -Q. \quad (4.10b)$$

277 These two expressions suggest that the two variables become equivalent by setting:

$$h = \hat{r}_c \hat{\alpha} a. \quad (4.11a)$$

278 Furthermore, for consistency of the large-scale vertical advection term (2nd on the left-hand side)
 279 in both equations (4.10a, b), a further constraint is required to establish the equivalence:

$$\hat{\alpha} = 1/\hat{r}_L. \quad (4.11b)$$

280 By further referring to the definition of $\hat{\alpha}$ in Eq. (4.8c), this condition simply reduces to

$$\alpha = 1. \quad (4.11c)$$

281 Recall from Sec. 4.b that the parameter α measures the efficiency of convection in modifying the
 282 stratification of the atmosphere.

283 The equivalence between CAPE (PEC) and the height in the shallow-water analogue atmosphere
 284 has been pointed out by Mapes (1998). We just establish this connection in a more formal manner.
 285 As a result, there is no longer a need to consider the time evolution of PEC, a , separately.

286 Consequently Eq. (4.9a) describes the convective-scale process, alongside the equation set (4.7a,
 287 b, c) for the large scale. With the help of Eq. (4.11a), the PEC can be eliminated from Eq. (4.9a)
 288 which becomes:

$$\hat{\epsilon} \frac{\partial k_c}{\partial t} = \hat{\alpha} h k_c - \frac{k_c}{\tilde{\tau}_D}, \quad (4.12a)$$

289 where

$$\tilde{\tau}_D = \tau_D^*/\hat{r}_c\hat{\alpha}^2 = \tau_D/\hat{r}_c\hat{\alpha}^2\tau_c \sim 10^4, \quad (4.12b)$$

$$\hat{\epsilon} = \hat{r}_c^2\hat{\alpha}^2 \sim 10^{-6}. \quad (4.12c)$$

290 Large and small values for these two parameters suggest shorter time scales involved with convection
291 compared to those of the large scale.

292 *e. Full System with Nonlinearity*

293 It remains to add nonlinearity to the linear version of the large-scale system derived so far,
294 Eqs. (4.7a, b, c). This final step turns out to be rather involved, and the details are presented in the
295 Appendix. Therein, we examine the physical consistency of the included nonlinear terms with the
296 energy cycle of the system. Based on those examinations, we adopt the final large-scale equation
297 set to be:

$$\frac{\partial u}{\partial t} + u \frac{\partial u}{\partial x} = -\frac{\partial h}{\partial x}, \quad (4.13a)$$

$$\frac{\partial h}{\partial t} + \frac{\partial u}{\partial x} = -Q, \quad (4.13b)$$

$$w = -\hat{r}_L \frac{\partial u}{\partial x}. \quad (4.13c)$$

298 Thus, the nonlinear advection term has been added only to the momentum equation (4.13a), but
299 not to the continuity (heat) equation (4.13b).

300 In summary, the full nonlinear system consists of Eqs. (4.13a, b, c) and (4.12a).

301 **5. Steady Solutions**

302 We first examine the steady solutions. This serves two purposes: i) to define a basic state of the
303 system, as a first step for performing perturbation analyses; and ii) to seek for the possibility of a
304 solution with a steady circulation, as an idealized analogue of the Hadley–Walker circulation.

305 The steady heat budget of the system is obtained by substituting Eqs. (4.13c) and (4.8a) into
306 Eq. (4.13b):

$$\bar{w} - \alpha\bar{w}_c + \hat{r}_L\hat{Q}_R = 0$$

307 or

$$\bar{w} - \alpha \bar{k}_c + \alpha w_R = 0 \quad (5.1)$$

308 Here, the overbars are added to denote a steady state. Also keep in mind that we retain two notations
309 with $k_c = w_c$.

310 The equilibrium state of convection is obtained from (4.12a) as:

$$\bar{k}_c = \bar{w}_c = 0 \quad \text{or} \quad \bar{h} = 1/\hat{\alpha}\tilde{\tau}_D \sim 10^{-3}. \quad (5.2a, b)$$

311 In the following, we take the second choice (5.2b), which is only a matter of adding a constant
312 height on perturbations. The first choice (5.2a) is less interesting with no possibility of convection
313 in the basic state.

314 From the heat balance (5.1), we see that \bar{w} and \bar{w}_c can be chosen freely so long they are consistent
315 with the dynamics. To seek a more specific solution, we set:

$$\bar{u} = \bar{u}_0 \sin kx \quad (5.3a)$$

316 with \bar{u}_0 a constant. Its substitution into the continuity equation (4.13c) leads to:

$$\bar{w} = -\bar{w}_0 \cos kx \quad (5.3b)$$

317 with $\bar{w}_0 = \hat{r}_L k u_0$. Furthermore, from Eq. (5.1),

$$\bar{w}_c = w_R - \frac{\bar{w}_0}{\alpha} \cos kx. \quad (5.3c)$$

318 To maintain the convective vertical velocity to be always positive definite, *i.e.*, $\bar{w}_c \geq 0$, we require
319 $w_R \geq \bar{w}_0/\alpha$. If we further assume the minimum convective velocity to be zero, we obtain $\bar{w}_0 = \alpha w_R$.

320 Finally, the steady nonlinear momentum equation,

$$\frac{\partial \bar{u}^2}{\partial x} = -\frac{\partial \bar{h}}{\partial x},$$

321 must be satisfied. However, here we face a problem: by the convective equilibrium condition, we
 322 have already set \bar{h} to be constant by Eq. (5.2b), and thus the right-hand side vanishes from the
 323 above, and there is no term to balance with the nonlinear advection on the left-hand side. We
 324 circumvent this difficulty by noting that the nonlinear advection term arising from a baroclinic
 325 circulation, actually projects onto a barotropic mode, and thus the height perturbation required to
 326 balance the right-hand side is also of a barotropic mode:

$$\frac{\partial \bar{u}^2}{\partial x} = -\frac{\partial \bar{h}_b}{\partial x},$$

327 with the subscript b standing for the barotropic mode, but also suggesting that this mode arises
 328 directly from the surface-boundary effect, *e.g.*, the SST distribution, partially reminiscent of the
 329 idea of Lindzen and Nigam (1987). The barotropic height field which balances with the nonlinear
 330 term is given by:

$$h_b = \frac{u_0^2}{4} (\cos 2kx - 1).$$

331 The short analysis of this section outlines very crudely how a consistent theory for steady tropical
 332 circulations can be developed in the context of a shallow-water analogue formulations: for further
 333 analyses we refer to *e.g.*, Gill (1980), Lindzen and Nigam (1987), Neelin and Held (1987), Yano
 334 (2023).

335 6. Linear Analysis

336 For performing perturbation analyses in the following two sections, we assume a homogeneous
 337 basic state with no large-scale circulation, *i.e.*, $\bar{u} = \bar{w} = 0$. The basic-state height is defined by
 338 Eq. (5.2b), and from Eq. (5.1), $\bar{w}_c = w_R = 1$, also recalling $\alpha = 1$ (*cf.*, Eq. 4.11c).

339 The resulting set of linear perturbation equations is:

$$\frac{\partial u'}{\partial t} = -\frac{\partial h'}{\partial x} \tag{6.1a}$$

$$\frac{\partial h'}{\partial t} + \frac{\partial u'}{\partial x} + \hat{\alpha} w'_c = 0 \tag{6.1b}$$

$$\hat{\epsilon} \frac{\partial w'_c}{\partial t} = \hat{\alpha} h' \tag{6.1c}$$

340 with the prime sign, \prime , denoting perturbation variables, and $w'_c = k'_c$.

341 We further assume a solution of the form, $\sim e^{i(kx+\omega t)}$. Then, the linear frequency is given by:

$$\omega^2 = k^2 + \hat{\alpha}^2 / \hat{\epsilon}$$

342 OR

$$\omega^2 = k^2 + \frac{1}{\hat{r}_c^2}. \quad (6.2)$$

343 Note that only a neutral wave solution is available, and the standard gravity–wave solution is
 344 recovered by setting $\hat{r}_c \rightarrow \infty$. Since $\hat{r}_c = \tau_c / \tau_L$ this limit corresponds to setting the convective
 345 time scale much longer than that of the large scale. Rather unintuitively, the presence of finite
 346 convective time scale (*i.e.*, τ_c finite) increases the frequency of the mode to be larger than that of
 347 the dry gravity wave: by further decreasing τ_c , the waves propagate faster. Note that in absence of a
 348 large–scale circulation, the system reduces to a linear version of the convective discharge–recharge
 349 system (*cf.*, Yano and Plant 2012b);

$$\begin{aligned} \frac{\partial h'}{\partial t} + \hat{\alpha} w'_c &= 0, \\ \hat{\epsilon} \frac{\partial w'_c}{\partial t} &= \hat{\alpha} h'. \end{aligned}$$

350 This leads to an oscillating solution with $\omega = \hat{\alpha} / \hat{\epsilon}^{1/2} = 1 / \hat{r}_c = \tau_L / \tau_c$. Effectively, the dispersion
 351 (6.2) is comprised of the square sum of the dry and convective frequencies.

352 7. Weakly Nonlinear Analysis

353 As an extension to the analysis of the last section, we now take into account a weak nonlinearity.
 354 For the purpose of developing a weakly–nonlinear formulation in a formal manner, we introduce an
 355 explicit perturbation parameter, which we choose to be $\hat{\epsilon}$, bearing in mind the numerical estimate
 356 of (4.12c). We also focus on the situation in which the system satisfies the free–ride balance

$$\frac{\partial u'}{\partial x} + \hat{\alpha} w'_c = 0 \quad (7.1)$$

357 (*cf.*, Fraedrich and McBride 1989) to the leading order of Eq. (4.13b). This state, alternatively
 358 called the weak-temperature gradient approximation (Sobel *et al.* 2001), can also be considered to
 359 be a quasi-equilibrium closure under the given shallow-water formulation.

360 To obtain (7.1) to the leading order, the variables must be re-scaled. It is found that appropriate
 361 re-scalings are:

$$h = \bar{h} + \hat{\epsilon}^3 h', \quad (7.2a)$$

$$w_c = \bar{w}_c + \hat{\epsilon} w'_c, \quad (7.2b)$$

$$u = \hat{\epsilon}^{3/2} u', \quad (7.2c)$$

362 and

$$\partial/\partial t = \hat{\epsilon} \partial/\partial \tau \quad (7.2d)$$

$$\partial/\partial x = \hat{\epsilon}^{-1/2} \partial/\partial \xi \quad (7.2e)$$

363 Thus, a longer time and shorter horizontal scales are introduced compared to the original nondi-
 364 mensionalization scales. Recall that \bar{h} is defined by Eq. (5.2b).

365 After substituting these re-scalings into the full set of equations, we obtain to the leading order
 366 of Eqs. (4.12a) and (4.13a):

$$\frac{\partial u'}{\partial \tau} + u' \frac{\partial u'}{\partial \xi} = -\frac{\partial h'}{\partial \xi}, \quad (7.3a)$$

$$\frac{\partial w'_c}{\partial \tau} = \hat{\alpha} h'. \quad (7.3b)$$

367 From Eqs. (7.1) and Eqs. (7.3b), we find:

$$w'_c = -\frac{1}{\hat{\alpha}} \frac{\partial u'}{\partial \xi}, \quad (7.4a)$$

$$h' = \frac{1}{\hat{\alpha}} \frac{\partial w'_c}{\partial \tau}. \quad (7.4b)$$

368 Substituting those expressions into Eq. (7.3a), we obtain a single equation for u' :

$$\frac{\partial u'}{\partial \tau} + u' \frac{\partial u'}{\partial \xi} - \hat{\alpha}^{-2} \frac{\partial^3 u'}{\partial \xi^2 \partial \tau} = 0. \quad (7.5)$$

369 Let us examine the linearized equation briefly:

$$\frac{\partial}{\partial \tau} \left(1 - \hat{\alpha}^{-2} \frac{\partial}{\partial \xi^2} \right) u' = 0,$$

370 which has the dispersion relation:

$$\omega(k^2 + \hat{\alpha}^2) = 0. \quad (7.6)$$

371 Thus, possible solutions are $\omega = 0$ and $k^2 = -\hat{\alpha}^2$. Keep in mind that the horizontal wavenumber, k ,
 372 is defined in terms of the re-scaled horizontal scale. Thus, only evanescent waves are available in
 373 the linear limit with the frequency left undetermined. As argued in *e.g.*, Yano and Flierl (1994), and
 374 Yano and Tribbia (2017), linear evanescent waves can be consistent solutions only if nonlinearity
 375 becomes important at a certain part of the system.

376 To solve the nonlinear equation (7.5), it is worthwhile to note that it has a similar form to the
 377 Kortewig–de Vries equation (*cf.*, Secs. 13.11 and 13.12 of Whitham 1974, Part 2, Epilogue of
 378 Lighthill 1978):

$$\frac{\partial u}{\partial t} + u \frac{\partial u}{\partial x} + \frac{\partial^3 u}{\partial x^3} = 0.$$

379 The latter is known to have a soliton solution:

$$u = 12k^2 \operatorname{sech}^2[k(x - x_0 - 4k^2t)]$$

380 Here, recall that $\operatorname{sech} x = \cosh^{-1} x$, and k and x_0 are arbitrary constants, which adjust the solution
 381 form. Thus, we anticipate that a solution with a similar form may also be available with Eq. (7.5).

382 To seek this possibility, we set

$$u' = u_0 \operatorname{sech}^2[k(\xi - \xi_0) - \omega\tau]$$

383 with u_0 , k , ω the parameters to be determined. Its substitution into Eq. (7.5) yields:

$$u_0 = 6\omega/\hat{\alpha}, \quad (7.7a)$$

$$k = \hat{\alpha}/2, \quad (7.7b)$$

384 while ω remains an arbitrary constant. The final solutions are:

$$u' = \frac{6\omega}{\hat{\alpha}} \operatorname{sech}^2 \varphi, \quad (7.8a)$$

$$w'_c = \frac{6\omega}{\hat{\alpha}} \operatorname{sech}^3 \varphi \sinh \varphi, \quad (7.8b)$$

$$h' = \frac{6\omega^2}{\hat{\alpha}^2} (-3\operatorname{sech}^4 \varphi + 2\operatorname{sech}^2 \varphi) \quad (7.8c)$$

385 with

$$\varphi = \frac{\hat{\alpha}}{2} (\xi - \xi_0) - \omega\tau. \quad (7.9)$$

386 Note that the wavenumber, k , of the solitary-wave solution is controlled by $\hat{\alpha}$, which is proportional
 387 to the ratio of the two horizontal scales, *i.e.*, $\hat{\alpha} = \alpha/\hat{r}_L = \alpha L/L_D$. Also recall the stretching factor,
 388 $\hat{\epsilon}^{-1/2}$, applied to the horizontal coordinate. Thus, a characteristic horizontal scale of this solitary
 389 wave is inferred by writing:

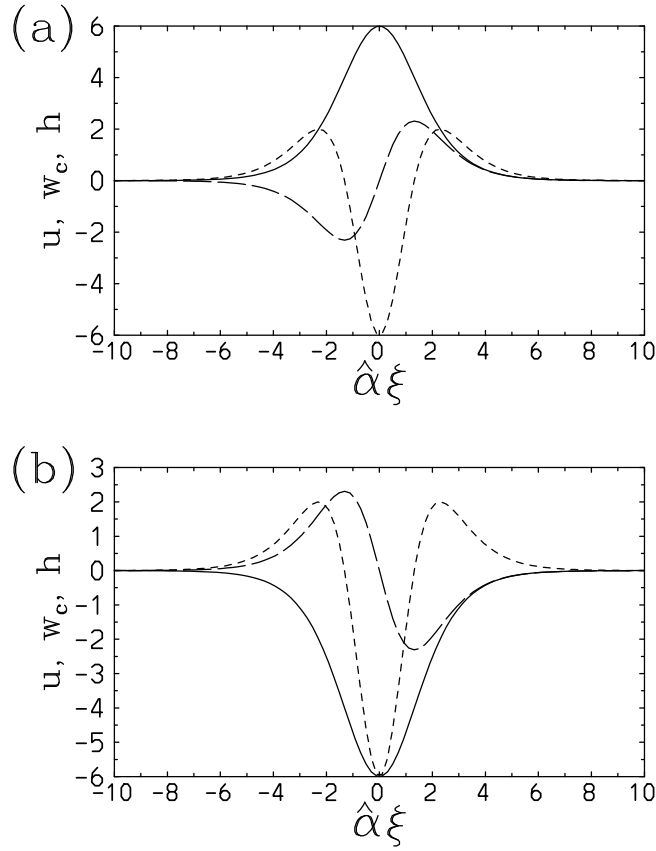
$$\hat{\alpha}\xi = \hat{\alpha}\hat{\epsilon}^{-1/2}x$$

390 From Eq. (4.12b), $\hat{\epsilon} = \hat{r}_c^2 \hat{\alpha}^2$, so that

$$\hat{\alpha}\xi = \frac{x}{\hat{r}_c} = x \frac{\tau_L}{\tau_c} = \frac{Lx}{c_g \tau_c},$$

391 also recalling the definitions (4.9c) and (4.6c). Bearing in mind that Lx is the dimensional length of
 392 the system, a characteristic wavelength of the solitary wave solution is identified as: $c_g \tau_c \sim 50$ km.
 393 Thus, this wave is typically localized to the mesoscale.

394 Also note that the velocity and the height, respectively, are scaled by the factors, $\omega/\hat{\alpha}$ and
 395 $\omega^2/\hat{\alpha}^2$. Thus, the wave amplitude increases with its frequency, ω , and in a more acerbated
 396 manner for the height than the velocities. More significantly, the westerly and easterly-wind
 397 bursts propagate eastwards and westwards, respectively. In particular, the overall behavior of the



403 FIG. 1. Examples of the solitary-wave solutions (7.8a, b, c) with $\hat{\alpha} = 1$: (a) eastward propagating with $\omega = 1$,
 404 and (b) westward propagating with $\omega = -1$: the horizontal coordinate is $\hat{\alpha}\xi = \hat{\alpha}\hat{\epsilon}^{-1/2}x$ with the unit scale of about
 405 50 km.

398 eastward-propagating solution is consistent with that of observed tropical westerly-wind bursts
 399 (*e.g.*, Hartten 1996, Yano *et al.* 2004).

400 Examples of the solutions with (a) $\omega = 1$ and (b) $\omega = -1$ are shown in Fig. 1. Here, curves are
 401 for the zonal wind, u' (solid), convection anomaly, w'_c (long dash), and the height, h' (short dash)
 402 with the horizontal coordinate given by $\hat{\alpha}\xi = \hat{\alpha}\hat{\epsilon}^{-1/2}x$.

406 8. Further Discussions

407 Atmospheric precipitating convection goes through a distinguished life cycle from a genesis
 408 to decay, and thus it is natural to expect that the convective life cycle may play an important
 409 role in its coupling to large-scale dynamics, especially over the tropics. From this perspective,
 410 the basic assumption of convective quasi-equilibrium adopted in convection parameterizations is

411 unsatisfactory, because this approximation totally neglects life cycles associated with parameterized
412 convection.

413 The present work shows what happens when a life cycle of convection is explicitly taken into
414 account as a *part* of the large-scale dynamics. A qualitative consequence, even without performing
415 any calculations, can even be intuitively expected: the short periodicity of convective life cycles
416 dominate aspects of the coupled dynamics. This expected tendency is more explicitly demonstrated
417 by a linear analysis, which shows that the squared frequency of a linear wave is obtained by a squared
418 sum of the characteristic frequency of the convective life cycle and a dry gravity-wave frequency,
419 under an analysis assuming no Coriolis force.

420 The convective life cycle used in the present study is based on the convective energy cycle
421 originally introduced by Arakawa and Schubert (1974), in seeking a basis for a closure of their
422 mass-flux parameterization. The energy cycle is closed by following Yano and Plant (2012b). The
423 large-scale dynamics adopted is a shallow-water analogue.

424 The high-frequency characteristic of convectively-coupled waves obtained with explicit convective
425 life cycles is in marked contrast to the typical characteristic under standard formulations with a
426 convective quasi-equilibrium assumption. In the latter case, convection is found to slow down the
427 dry large-scale waves by decreasing the effective stratification of the atmosphere. This behavior
428 arises because any explicit periodicities associated with convection are effectively eliminated by
429 averaging them out through the convective quasi-equilibrium assumption. The approach of the
430 present paper explicitly retains such a high convective-scale frequency, and thus this frequency is
431 added to a full spectrum of the whole system. An explicit emergence of the convective-scale high
432 frequencies into the large-scale dynamics is obviously an unfavorable feature if the focus of an
433 analysis is on the long timescale phenomena.

434 A more attractive feature emerges when the system is scaled down to a mesoscale regime, also
435 introducing a weak nonlinearity. This re-scaling is performed in such a manner that the free-ride
436 balance (Fraedrich and McBride 1989: see also Sobel *et al.* 2001) is obtained to the leading order.
437 The analysis leads to a nonlinear equation analogous to the Kortweg-de Vries equation, and like
438 the latter, it contains a solitary-wave solution. The obtained mesoscale solution is reminiscent of
439 tropical westerly–wind bursts.

440 Although an analysis with the rotation effect is still to be performed, it is evident that the
441 eastward-propagating solitary gravity wave solution obtained can be re-interpreted as a Kelvin
442 wave in the presence of rotation so long as we can assume that the equatorial deformation radius
443 is much larger than the longitudinal wavelength. Nevertheless, a full analysis of this system with
444 the rotation effect will be worthwhile to explore rich possibilities of nonlinear interactions between
445 convective life cycles and the equatorial waves. This investigation may also be considered a natural
446 extension of dry solitary equatorial waves as investigated by Boyd (1980, 1983, 1984, 1985).

447 **9. Conclusions**

448 The most important lesson to learn from the present study is that if the focus is solely on the
449 global scale of the atmosphere, then one should not try to include a convective life cycle explicitly
450 into a model, how attractive this approach might appear to be at first sight.

451 On the other hand, for those who wish to investigate tropical atmospheric dynamics in its full
452 spectrum, the convective energy-cycle system coupled with large-scale dynamics provides an
453 attractive option to pursue. Although only a preliminary investigation has been performed, an
454 identified solitary-wave solution, reminiscent of tropical westerly-wind bursts, already suggests a
455 rich behavior of this system under full nonlinearity. However, we should also keep in mind that
456 convection is still parameterized, using a mass-flux-based formulation.

457 **Data Availability**

458 No data is used in the present study.

459 **Appendix: Energy Cycle Analysis**

460 The purpose of this Appendix is identify the physically most consistent form of nonlinearity for
461 the shallow-water analogue system from the point of view of the energy-cycle of the system. The
462 most straightforward way to add nonlinearity to the linear large-scale system (4.7a, b, c) would be

463 in the identical form as that which appears in the actual shallow-water system:

$$\frac{\partial u}{\partial t} + u \frac{\partial u}{\partial x} = -\frac{\partial h}{\partial x}, \quad (\text{A.1a})$$

$$\frac{\partial h}{\partial t} + \frac{\partial}{\partial x} u(1+h) = -Q, \quad (\text{A.1b})$$

$$w = -\hat{r}_L \frac{\partial u}{\partial x}. \quad (\text{A.1c})$$

464 Here, we are going to show that this form leads to a physically unacceptable interpretation from
 465 the point of view of the energy cycle. We show further that the problem arises with the postulated
 466 nonlinear contribution to Eq. (A.1b) but that the nonlinear advection term in Eq. (A.1a) may be
 467 retained.

468 *a. Kinetic Energy*

469 To derive the kinetic–energy budget, we first re-write the momentum equation (A.1a) in a flux
 470 form by multiplying it by $h_T = 1 + h$, and adding by Eq. (A.1b) multiplied by u :

$$\frac{\partial u h_T}{\partial t} + \frac{\partial}{\partial x} u^2 h_T = -\frac{\partial}{\partial x} u h_T^2 - u Q. \quad (\text{A.2})$$

471 Multiplying Eq. (A.1a) by $u h_T$ and Eq. (A.2) by u , we obtain the budget:

$$\frac{\partial}{\partial t} \frac{h_T}{2} u^2 + \frac{\partial}{\partial x} \frac{h_T u^3}{2} = -u \frac{\partial}{\partial x} \frac{h_T^2}{2} - \frac{u^2}{2} Q. \quad (\text{A.3})$$

472 Here is the first key point to note: from a physical consideration, we expect that the large–scale
 473 kinetic energy would *not directly* be modified by a convective process or by diabatic heating. Thus,
 474 Eq. (A.3) is not physically consistent by containing a source term due to diabatic heating.

475 We can trace this physical inconsistency to the fact that the kinetic energy is defined by $h_T u^2/2$
 476 above. Although this is a physically consistent definition of kinetic energy in the original shallow–
 477 water system, that is no longer the case for this shallow–water analogue atmosphere. This con-
 478 clusion stems from the fact that in the shallow–water analogue atmosphere, the height is better
 479 interpreted as a representation of the potential-temperature anomaly rather than a representation of
 480 a fluid depth, as in the original definition of the shallow–water system.

481 Based on this consideration, we conclude that the kinetic energy is better defined as $u^2/2$. With
 482 this definition, the kinetic–energy budget is obtained by multiplying Eq. (A.1a) by u :

$$\frac{\partial u^2}{\partial t} \frac{1}{2} + \frac{\partial u^3}{\partial x} \frac{1}{3} = -u \frac{\partial h}{\partial x}. \quad (\text{A.4})$$

483 Here, the form of the divergence term is rather unfortunate, and a minor negative consequence
 484 from the redefinition.

485 *b. Potential Energy*

486 A similar consideration also applies when defining the potential energy of this shallow–water
 487 analogue system. As already suggested above, the total depth, h_T , of the system does not have
 488 much physical significance: it is better to take the height perturbation, h , as a measure of the
 489 potential temperature perturbation, θ , under the relation (3.12b). Thus, it also follows that the
 490 potential energy is better defined by $h^2/2$ rather than $h_T^2/2$. Its budget is obtained by multiplying
 491 Eq. (A.1b) by h , so that:

$$\frac{\partial h^2}{\partial t} \frac{1}{2} + h \frac{\partial}{\partial x} u h_T = -hQ. \quad (\text{A.5})$$

492 We may note above that the advection term does not turn into a flux form as expected.

493 *c. Total Energy Budget*

494 Finally, by taking sum of Eqs. (A.4) and (A.5), we obtain the conservation law of the total energy
 495 as:

$$\frac{\partial}{\partial t} \left(\frac{u^2 + h^2}{2} \right) + \frac{\partial}{\partial x} \frac{u^3}{3} + h \frac{\partial}{\partial x} u h_T + u \frac{\partial h}{\partial x} = -hQ.$$

496 To express the last two terms on the left–hand side closer to a flux form, recall that $h_T = 1 + h$, thus

$$h \frac{\partial}{\partial x} u h_T + u \frac{\partial h}{\partial x} = \frac{\partial}{\partial x} u h + h \frac{\partial}{\partial x} u h.$$

497 We can recognize that the remaining non–flux term on the left–hand side arises from the nonlinear
 498 term in the height equation (A.1b). This result suggests that it is unphysical to add a nonlinear
 499 advection term to the height (heat) equation under the present shallow–water analogue formulation.
 500 Thus, the choice of the form (4.13b) follows. After this modification, the total–energy conservation

501 law reduces to:

$$\frac{\partial}{\partial t} \left(\frac{u^2 + h^2}{2} \right) + \frac{\partial}{\partial x} \left(\frac{u^3}{3} + uh \right) = -hQ. \quad (\text{A.6})$$

502 *d. Coupling with Convection*

503 The final step is to add the convective kinetic energy to the energy budget (A.6) just obtained.
504 Towards this goal, note first that the term hQ on the right-hand side of the potential energy budget
505 (A.5) can be re-written with the help of Eq. (4.8a) as:

$$hQ = \hat{\alpha} h k_c - h\hat{Q}_R. \quad (\text{A.7})$$

506 Hence, convective kinetic energy is generated (i.e., $\hat{\alpha} h k_c > 0$ on the right hand side of Eq. 4.12a)
507 by consuming the potential energy (i.e., $hQ > 0$ through the same process: the right-hand side of
508 Eq. A.5). By substituting the expression (A.7) into the right-hand side of Eq. (A.6), we obtain:

$$\frac{\partial}{\partial t} \left(\frac{u^2 + h^2}{2} \right) + \frac{\partial}{\partial x} \left(\frac{u^3}{3} + uh \right) = -\hat{\alpha} h k_c + h\hat{Q}_R. \quad (\text{A.8})$$

509 Taking the sum of Eqs. (A.8) and (4.12a), the total-energy budget including the contribution of
510 the convective scale is:

$$\frac{\partial}{\partial t} \left(\frac{u^2 + h^2}{2} + \hat{\epsilon} k_c \right) + \frac{\partial}{\partial x} \left(\frac{u^3}{3} + uh \right) = h\hat{Q}_R - \frac{k_c}{\tilde{\tau}_D}. \quad (\text{A.9})$$

511 Thus, as a whole the radiation, \hat{Q}_R , is the only ultimate source of the energy to the system, and
512 the only sink is the dissipative loss, $k_c/\tilde{\tau}_D$, of convective kinetic energy. Note that the large-scale
513 dynamics has been assumed to be dissipationless for simplicity.

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