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Article

Harmonics Mitigation Based on the Minimization of Non-Linearity Current in a Power System

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Abstract: Harmonic issues in power systems are becoming an important topic for industrial customers and power suppliers alike due to their adverse effects in both consumer appliances as well as for utility suppliers. Consumers should seek to reduce harmonic pollution, regardless of voltage or current distortion already present in the network. This article suggests a new method for suppressing distortions by using the non-linearity current index (*NLCI*) to determine the shunt single-tuned passive filter (STPF) compensator value in non-sinusoidal power systems, with the objective of maintaining the power factor within desired limits. The objective of the proposed method is to minimize the nonlinear current of customer's loads in the power system at the point of common coupling (PCC). Moreover, the proposed design takes into consideration other practical constraints for the total voltage and individual harmonic distortion limits, ensuring compliance with (Institute of Electrical and Electronics Engineers) IEEE 519-2014 guidelines, maintaining distortions at an acceptable level while also abiding by the capacitor loading constraints established in IEEE 18-2012. The performance of the optimally designed compensator is assessed using well documented IEEE standards based on numerical examples of nonlinear loads taken from previous publications.

Keywords: power factor; harmonics; single-tuned passive filter; non-linearity current index

1. Introduction

In recent years, there have been serious concerns regarding the quality of available power in electrical networks, making this issue a significant focus of research interest for both suppliers and users. Power system harmonics are considered one of the most important issues because of their reduction in power quality in power systems [1–3]. This is due to the widespread nonlinear loads exhibited across different appliances (such as variable frequency drives and switching mode power supplies), which can result in distortion currents with a frequency greater than the fundamental frequency. These harmonics can have detrimental effects on other components of the power system across all electrical sectors. Some of these effects are immediate (i.e., noise, interference, and control circuits, etc.) while others are long-term (i.e., heating due to extra power losses, damage). Furthermore, they lead to the degradation of the load power factor and higher transmission line losses, and thus contribute to a reduction in the efficiency of the transmission network. Thus, it is clear that harmonic levels should be minimized by all participants in the electrical grid [4–7]. There are different approaches to mitigating the effects of harmonics problems, such as load conditioning, which ensures that the electrical equipment is less sensitive to power disturbances. Other approaches used involve adding filters to the line power system, either in series or shunt connections. Harmonic mitigation techniques such as the K-factor transformer and shifting transformer are also applied in order to limit the power quality problem [8–10]. Industrial electrical systems contain the majority of medium- to high-powered contaminant sources, often in the form of static power converters and electric arc furnaces. In such systems, single objective filter

solutions are usually preferred, to attempt to comply with the relevant power quality standards while incurring the least costs [11]. Adding harmonic filters (passive and/or active) is the most frequently used approach [12–16]. Further, passive filters are deemed to be the most effective and viable solution for mitigating harmonics in power systems. Therefore, they are broadly used in transmission and distribution power systems due to their simple design, cost effectiveness, simplicity in maintenance, and high reliability. Passive filters are characterized by having a dual purpose, reducing current harmonics and correcting the power factor (PF). Therefore, they have been recommended for reducing nonlinear current loads, especially for existing industrial users [6,17,18]. On the other hand, employing passive filters may introduce resonance into the power system; thus, they should be designed such that they are safely located away from existing power harmonics [19,20]. Passive filters can be classified into two general categories, namely (i) tuned passive filters, (single-tuned or double-tuned filters) and (ii) high-pass passive filters. These filters typically have two types of connection, either in series, which presents a high-impedance series path, or as shunt, which presents a low-impedance path. In this context, a shunt connection is generally preferred and used more often for harmonics reduction than the series connection due to its ability to support a range of voltages while also compensating reactive power at the fundamental frequency [2,6,21]. Figure 1 presents several configurations of shunt passive harmonic filters [17].

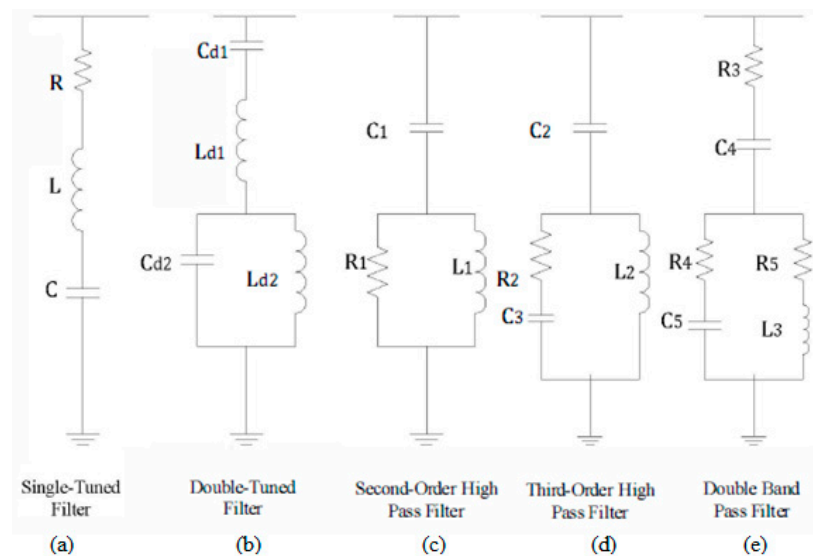


Figure 1. Several arrangements of passive filters [17].

Several studies have already addressed the problem of optimal filter design for harmonic mitigation in power systems. A single tuned passive filter compensator has been demonstrated to be an effective method of improving the power factor, as well as reducing power losses and decreasing voltage distortion to acceptable levels [22,23]. However, the design of passive power filters should be handled with caution as it is not a straightforward problem due to the contradictory requirements in power factor specifications, voltage total harmonic distortion (VTHD), and current total harmonic distortion (ITHD) [24].

In the literature, the maximization of the PF has received the highest priority as an objective during the design of optimal passive filters [25–27], while maximizing the load PF with minimum transmission loss has frequently been taken as a main objective for the design of the compensation elements of passive filters in order to achieve reasonable levels of total harmonic distortion (voltage) (THDV) [28,29]. However, maximizing PF alone may not succeed in minimizing the total harmonic distortion of both voltage and current, although it may work to reduce them. In contrast, another goal, e.g., [30] has been to minimize THDV, to obtain an optimal passive filter design which takes into consideration the non-linearity of the load, in which having the load PF at an acceptable, pre-specified

level is used as a constraint. A passive filter solution based on minimizing $THDV$ and total harmonic distortion current ($THDI$) in a power system has also been proposed in [31]; however, both obligations for capacitor loading as given in IEEE 18-2012 and the power supply characteristics, were neglected. $THDI$ and $THDV$ were also used to determine compensator values for passive filters [32] but the approach failed, albeit only just, to achieve the manufacturer's standard values for shunt capacitors. Different objectives have been used collectively in different combinations for the same goal, and these objectives include the maximization of PF and minimization of filter cost, $THDV$, and $THDI$ [33]. However, in considering such objectives, the nature of the supply source in any power system should always be considered when determining the optimal parameters for the design of passive filters.

In all the above studies, passive filters were designed to mitigate harmonics and correct the PF using different objective functions under distorted current load conditions. Such conventional objective functions do not distinguish between the current due to the mains supply distortion and the nonlinear current due to the industrial customer's loads at the PCC. However, the $NLCI$ (non-linearity current index) [34] is an objective function which does make this important distinction. The $NLCI$ depends on the likelihood that the supply system alone is responsible for the unbalanced and harmonic distortion at the PCC if the loads under test are linear and balanced. The $NLCI$ has been successfully evaluated to identify just the harmonic pollution responsibility at the PCC in a power system.

In this paper, a new approach is presented for minimizing $NLCI$, whereby it is required to keep the PF at the desired level, while considering the non-linearity of the loads. Other considerations have been taken into account, including the frequency-dependent nature of the power supply source and the resonant problems which may result from the compensator filter values. In this way, an optimum single-tuned passive filter (STPF) compensator is designed to minimize the expected value of $NLCI$ for a specified range of source harmonic and impedance values. Finally, examples from previous publications are discussed to illustrate and validate the contribution of the newly developed method.

The resonance phenomenon in a power system is the most critical issue when connecting an STPF to the network. Resonance issues (either series or parallel) arise at a frequency lower than the tuned frequency. Theoretically, the maximum efficiency is obtained if the STPF is tuned correctly to be equivalent to the harmonics frequency that has to be mitigated. Usually, the STPF is tuned between 3% and 10% of the series, and parallel resonance frequency to detune the effects. This provides a margin of safety in cases where high temperatures can lead to component failure or drifts in either capacitance or inductance nominal values [35,36].

2. Formulation of the $NLCI$ Minimized STPF

In this section, an example of a non-sinusoidal power system is presented after compensation with the newly designed STPF and the mathematical expressions to define $NLCI$ for the compensated system are presented. The major advantages of this approach are demonstrated since several relevant criteria have been taken into consideration in the proposed design when determining the STPF compensator values. The design accounts for the following:

1. The effect of transmission line impedance on the load voltage at the PCC.
2. Source nonlinearity is included in the problem formulation by incorporating as separate parameters the source harmonic current I_{Sh} and the source harmonic voltage V_{Sh} .
3. Load nonlinearity is included in the problem formulation as separate parameters, the harmonic load current I_{Lh} and the harmonic load voltage V_{Lh} .
4. The frequency dependence of the solution is taken into consideration.
5. Compensator values that would generate resonance phenomena are identified and excluded from the domain of possible solutions.

A typical industrial power system, such as the one given in Figure 2, is considered to describe a novel approach based on $NLCI$. The configuration used is similar to that used for a single-line design of single-tuned passive filters using the response surface methodology [24], it comprises a transformer,

the consumer loads (which include both linear and nonlinear loads) and the STPF filter connected to the PCC. Figure 3 describes the single-phase equivalent circuit of the industrial system under study with the novel shunt STPF providing compensation. In this circuit, the background voltage harmonic components are taken into account; these are represented by V_{Sh} . These voltage harmonic distortions affect a load bus at the PCC, which is which may be already suffering from extra current harmonic distortion due to nonlinear loads associated with the power distribution in the network.

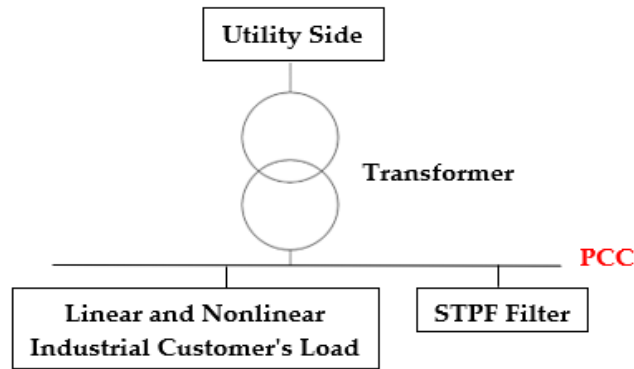


Figure 2. Single-line diagram representation of the emulated system (after [23]).

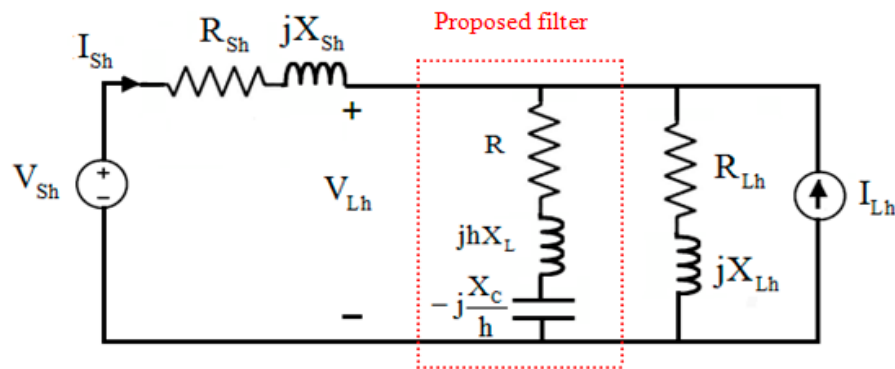


Figure 3. Single-phase equivalent circuit of the compensated system.

The *NLCI* based current source model is also described by the nonlinear load currents I_{Lh} , where subscript h represents the harmonic order.

A linear load, such as a motor, will draw a non-linear current, i.e., one containing harmonics, if the voltage is distorted. However, the motor is simply drawing a current that is proportional, at each frequency, to its source voltage, based upon its impedance. Only a motor fed by a purely 60 Hz source was found to draw a current without any harmonic content [36]. Therefore, at any harmonic order h , the voltage source presented by the mains power provider, and the harmonic current source presented by the nonlinear user load, are given as

$$v_s(t) = \sum_h v_{Sh}(t) \quad (1)$$

$$i_L(t) = \sum_h i_{Lh}(t) \quad (2)$$

Furthermore, the source impedance (short-circuit impedance) Z_{Sh} and load impedance Z_{Lh} can be respectively expressed as

$$Z_{Sh} = R_{Sh} + jX_{Sh} \quad (3)$$

$$Z_{Lh} = R_{Lh} + jX_{Lh} \quad (4)$$

where R_{Sh} and X_{Sh} represent the Thevenin source resistance and reactance, respectively; and R_{Lh} represents the load resistance; and X_{Lh} represents the load reactance. All are given in ohms at harmonic order h .

The harmonic compensator impedance for the STPF at the h^{th} harmonic is given as

$$Z_{Ch} = R + jX_F \quad (5)$$

$$X_F = hX_L - \frac{X_C}{h} \quad (6)$$

where X_L is the magnitude of the inductive reactance of the shunt filter at the fundamental frequency, X_C is the magnitude of the capacitive reactance of the STPF at the fundamental frequency, R is the filter's internal resistance and X_F is the total complex filter reactance.

Following this analysis, the h^{th} harmonic linear current (I_{linh}) drawn by the ideal load and the compensated load voltage (V_{Lh}) at each harmonic number (h) are expressed as follows:

$$I_{linh} = \frac{A + jB}{[D_{Rh}] + j[D_{Jh}]} \quad (7)$$

$$V_{Lh} = \frac{N_{Rh} + jN_{Jh}}{D_{Rh} + jD_{Jh}} \quad (8)$$

where

$$A = [V_{Sh}(R + R_{Lh}) + I_{Lh}R_{CLh} - I_{Lh}(R_{TLh} - X_F(X_{Lh} + X_{Sh}) + R(R_{Sh} + R_{Lh}))] \quad (9)$$

$$B = [V_{Sh}(X_F + X_{Lh}) + I_{Lh}X_{CLh} - I_{Lh}(X_{TLh} + R(X_{Sh} + X_{Lh}) + X_F(R_{Lh} + R_{Sh}))] \quad (10)$$

$$D_{Rh} = R_{TLh} - X_F(X_{Lh} + X_{Sh}) + R(R_{Sh} + R_{Lh}) \quad (11)$$

$$D_{Jh} = X_{TLh} + R(X_{Sh} + X_{Lh}) + X_F(R_{Lh} + R_{Sh}) \quad (12)$$

$$N_{Rh} = V_{Sh}R_{CLh} - I_{Lh}(R_{TLh} - X_F X_{TLh}) \quad (13)$$

$$N_{Jh} = V_{Sh}X_{CLh} - I_{Lh}(R X_{TLh} + X_F R_{TLh}) \quad (14)$$

so that,

$$R_{CLh} = R R_{Lh} - X_{Lh} X_F \quad (15)$$

$$X_{CLh} = R X_{Lh} + R_{Lh} X_F \quad (16)$$

$$R_{TLh} = R_{Sh} R_{Lh} - X_{Lh} X_{Sh} \quad (17)$$

$$X_{TLh} = R_{Lh} X_{Sh} + R_{Sh} X_{Lh} \quad (18)$$

Then, one can define $NLCI$ for the compensated system, as follows:

$$NLCI = 1 - \frac{I_{lin}}{I_S} \quad (19)$$

In this study, the effects of the main sources of uncertainty and disturbance were analyzed using four different case studies. The first two cases represent the system with low short-circuit capacity (80 MVA) and the second two cases represent a high short-circuit capacity (150 VA). For each short circuit capacity, the first scenario (cases 1 and 3) represents the system with no background voltage distortion but with load current harmonic distortion; the second scenario (cases 2 and 4) represents the system with both voltage and current harmonic voltage distortion.

Five different power quality indices were considered to assess and analyze the compensated system performance:

The compensated load power factor (PF) is calculated as follows:

$$PF = \frac{P_L}{V_L I_S} = \frac{\sum_h G_{Lh} V_{Lh}^2}{\sqrt{\sum_h I_{Sh}^2 \sum_h V_{Lh}^2}} \quad (20)$$

where P_L is the load active power per phase in watts (W).

The compensated displacement power factor (DPF), which is expressed as follows:

$$DPF = \frac{P_{L1}}{V_{L1} I_{S1}} \quad (21)$$

(where subscript “1” stands for the fundamental h order).

The transmission power loss (TL), which is given as follows:

$$TL = \sum_h I_{Sh}^2 R_{Sh} \quad (22)$$

The transmission efficiency (η), which is defined as follows:

$$\eta = \frac{P_L}{TL + P_S} \quad (23)$$

where P_S is the supply active power per phase in W .

Voltage total harmonic distortion ($VTHD$), which has been introduced to identify the harmonic component at the load bus, is expressed as

$$VTHD = \frac{\sqrt{\sum_{h>1}^n V_{Lh}^2}}{V_{L1}} 100\% \quad (24)$$

It has been assumed that the resistance of the compensator reactance was ignored because of its small size with respect to the magnitude of its fundamental reactance [37].

3. Constraints

3.1. Formulation of the Harmonic Resonance Constraint

Harmonic resonances are considered as the most significant factor that should be taken into consideration while designing a shunt STPF. Parallel resonance can be expressed as a high impedance to the flow of harmonic current, while series resonance can be expressed as a low impedance [35].

It is necessary to determine the value of the inductor and capacitors (hX_L and X_C/h) in order to avoid resonances in the power system under study. Consequently, the compensator parameters resulting in a resonant phenomenon have to be identified and considered in the optimization problem in order to be excluded from the available search space.

The h^{th} equivalent impedance Z_{THK} as seen from the source-side, for the power system under study shown in Figure 3, is given as

$$Z_{THK} = Z_{Sh} + \left(\frac{Z_{Ch} Z_{Lh}}{Z_{Ch} + Z_{Lh}} \right) \quad (25)$$

Setting its imaginary part to zero and after some simplification, the resonance constraint equation is given as:

$$\alpha_{h1}\left(hX_L - \frac{X_C}{h}\right)^2 + \alpha_{h2}\left(hX_L - \frac{X_C}{h}\right) + \alpha_{h3} = 0 \quad (26)$$

where

$$\begin{aligned} \alpha_{h1} &= X_{Sh} + X_{Lh}, \\ \alpha_{h2} &= X_{Lh}^2 + R_{Lh}^2 + 2X_{Sh}X_{Lh}, \\ \alpha_{h3} &= X_{Sh}(R + R_{Lh})^2 + R^2X_{Lh} + X_{Sh}X_{Lh}^2. \end{aligned}$$

Solving for $(hX_L$ and $X_C/h)$,

$$X_F = hX_L - \frac{X_C}{h} = \frac{-\alpha_2 \pm \sqrt{\alpha_2^2 - 4\alpha_1\alpha_3}}{2\alpha_1} \quad (27)$$

where parameters α_i ($i = 1,2,3$) in (22) are associated with the quadratic equation in X_C and X_L for any given harmonic order in the search algorithm.

3.2. Shunt Capacitor Constraints Based on the IEEE 18-2012 Standard

An algorithm with built in provisions to identify and avoid compensator parameters of the passive filter would likely produce its own resonance. Under resonance conditions, the system with a filter can, therefore, be considerably worse than a system without filters. Hence the algorithm has been designed to arrive at the optimal filter solution that satisfies the limitations of the PF constraints taking into account the source and load nonlinearities. Furthermore, the algorithm has been developed to optimally satisfy the practical constraints for the voltage total harmonic distortion at the PCC between the mains and the industrial consumer limits in compliance with IEEE 519-2014 guidelines to below the 5.0% limit of $VTHD$, with each individual harmonic limited to 3%.

The design of the shunt STPF requires compliance with IEEE Standard 18-2012 [38], which states that shunt capacitors will be capable of continuous operation without exceeding the following limitations:

1. Not to exceed 135% of the nominal the square of the root mean square (rms) capacitor current I_C :

$$I_C = \sqrt{\sum_h I_{Ch}^2} \quad (28)$$

where the current of the capacitor (I_{Ch}) at the h^{th} harmonic is given as:

$$I_{Ch} = \frac{V_{Lh}}{Z_{CLh}} \quad (29)$$

2. Not to exceed 110 % of the nominal rms capacitor voltage (V_C):

$$V_C = \sqrt{\sum_h V_{Ch}^2} \quad (30)$$

where the voltage of the capacitor (V_{Ch}) at the h^{th} harmonic is given as:

$$V_{Ch} = I_{Ch} \frac{X_C}{h} \quad (31)$$

3. Not to exceed 120 % of the peak voltage (V_{CP}):

$$V_{CP} = \sum_h I_{Ch} \frac{X_C}{h} \quad (32)$$

4. Not to exceed 135 % of the nominal kvar (Q_C):

$$V_C = I_C V_C \quad (33)$$

3.3. Other Constraints Based on the IEEE 519-2014 Standard

Load power factor limits are taken into account due to some utilities imposing additional charges or penalties when the power factor is less than 90% or 95%, or for short periods of time up to 80% [35].

VTHD and ITHD expressed in (34) and (35), respectively, are considered the most common measurements used to represent the harmonic content waveform. Both are applied as constraints where the specifying limits are based on the IEEE 519-2014 Standard [39].

$$VTHD = \frac{\sum_{h>1}^n V_{Lh}^2}{V_{L1}} \quad (34)$$

$$ITHD = \frac{\sum_{h>1}^n I_{Sh}^2}{I_{S1}} \quad (35)$$

4. Optimization Technique and Search Algorithm

Minimization of the non-linearity current index (NLCI), measured at PCC, is proposed to represent the objective function for the optimal design parameter values of the filter. Maximizing PF enables the optimization of the STPF values, as it results to a passive filter design with an enhanced resonance damping ability. Both can be expressed as functions of the STPF filter parameters (X_C and X_L).

Thus, the objective functions of the filter design become as follows:

$$\text{Minimize } NLCI(X_{Ci} \text{ and } X_{Li}), \text{ subject to: } 90 \% \leq PF(X_{Ci} \text{ and } X_{Li}) \leq 100 \%$$

X_{Ci} and X_{Li} are excluded from the solution of Equation (27).

These nonlinear constraints limit PF within an acceptable specified range and avoid resonance. A general flow chart for the STPF search algorithm is demonstrated in Figure 4 using the feasible sequential quadratic programming (FFSQP) package. Optimal design of a filter often appears as a multi-factorial problem, because it generally contains different objectives with contradictory constraints pulling in different directions. FFSQP is ideal for this non-linear optimization design problem under conflicting design requirements [30].

The FFSQP search algorithm steps in sequence, defined for the objective function under consideration, were as follows:

1. Construct the needed subroutines (objective subroutine (f), constraints subroutine (g)) to develop the FFSQP search.
2. Construct other subroutines that describe the mathematical modelling of the system.
3. Run the search algorithm considering constraints.
4. Choose the first value of the reactive power Q_{Ci} rating of capacitor in kvar, so that $Q_{Ci} = \{Q_{C1}, Q_{C2} \dots Q_{Cj}\}$, where ΔQ_C or $(Q_{Cj} - Q_{Cj-1})$ is the kvar step. Also, j is the number of discrete values for the used voltage rating and i is a counter that has a starting value of 1.
5. Calculate X_{Ci} from $X_{Ci} = \frac{V_{S1}^2}{Q_{Ci}}$
6. Calculate X_{Li} from equation (27).
7. Run the search algorithm considering the filter component values to be the initial values at the beginning of each search in each region.
8. Find the local solutions that achieve the best fitness of the considered objective.

9. The algorithm will stop when a feasible point is reached or when the stopping criterion defined in terms of ε is met, where ε represents the relative difference in the objective function as a convergence-stopping criterion.
10. After stopping, scan through local solutions to get the global one.
11. Determine the filter parameters values corresponding to the global solution.

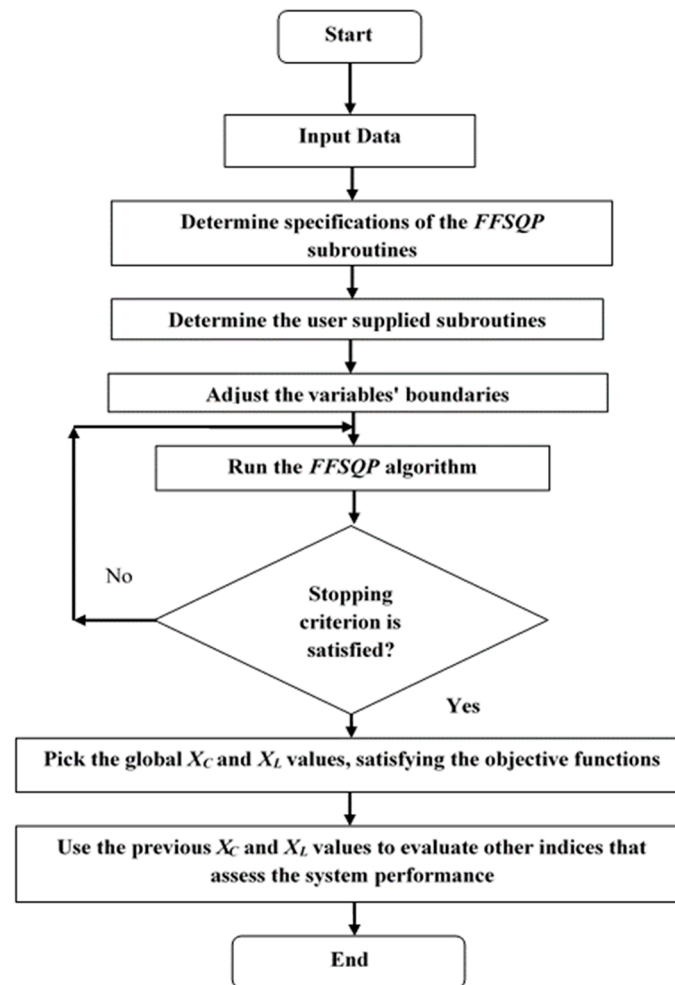


Figure 4. Flowchart of the FFSQP search algorithm.

5. Case Studies and Simulated Results

Four cases of an industrial power system [40,41] were simulated by applying the above-mentioned optimization method. Tables 1 and 2 show the numerical data and the corresponding industrial customer's loading, respectively [40,41], these values have been subsequently adopted in other IEEE publications [42] and other publications on the subject [43]. The inductive three-phase linear and nonlinear load group is 5100 kW and 4965 kvar with a *DPF* of 0.7165. The 60-cycle supply bus voltage is 4.16 kV (line-to-line). Table 1 also gives the uncompensated power system performance results which are comparable with the shunt STPF compensation results.

Table 1. Industrial plant parameters and source harmonics.

Parameters & Cases	Case 1	Case 2	Case 3	Case 4
MVA_{SC} (MVA)	80		150	
R_{S1} (Ω)	0.02163	0.02163	0.01154	0.01154
X_{S1} (Ω)	0.2163	0.2163	0.1154	0.1154
R_{L1} (Ω)	1.7421	1.7421	1.7421	1.7421
X_{L1} (Ω)	1.6960	1.6960	1.6960	1.6960
V_{S1} (V)	2400.00	2400.00	2400.00	2400.00
V_{S5} (V)	0.00	96.00	0.00	96.00
V_{S7} (V)	0.00	72.00	0.00	72.00
V_{S11} (V)	0.00	48.00	0.00	48.00
V_{S13} (V)	0.00	24.00	0.00	24.00
I_{L5} (A)	33	33	33	33
I_{L7} (A)	25	25	25	25
I_{L11} (A)	9	9	9	9
I_{L13} (A)	8	8	8	8
Uncompensated Indices				
PF (%)	71.57	71.48	71.58	71.48
DPF (%)	71.65	71.65	71.65	71.65
TL (kW)	18.44	18.45	10.47	10.48
η (%)	98.77	98.77	99.34	99.34

Table 2. Detailed industrial loadings.

Load Type	Active Power (kW)	Reactive Power (kvar)	PF (%)
Linear loads	1200	900	80.00
	900	918	80.00
Nonlinear loads	600	612	70.00
	1100	1902	50.00
Other loads	1300	630	90.00
Total loads	5100	4965	71.65

In Table 1, the first 2 rows show different power system parameters, subsequent 2 rows show the corresponding load parameters and all subsequent rows show the associated source and load harmonics. The first two cases (vertical columns) represent the system with low short-circuit capacity (80 MVA), while the third and fourth cases represent the system with high short-circuit capacity (150 MVA). For each short circuit capacity, the first scenario (Cases 1 and 3) represent the system with no background supply voltage distortion ($V_{S5} = 0$ V, $V_{S7} = 0$ V, $V_{S11} = 0$ V, $V_{S13} = 0$ V) but with load current harmonic distortion ($I_{L5} = 33$ A, $I_{L7} = 25$ A, $I_{L11} = 9$ A, $I_{L13} = 8$ A); the second scenario (Cases 2 and 4) represents the system with both voltage and current harmonic distortion ($V_{S5} = 96$ V, $V_{S7} = 72$ V, $V_{S11} = 48$ V, $V_{S13} = 24$ V) and ($I_{L5} = 33$ A, $I_{L7} = 25$ A, $I_{L11} = 9$ A, $I_{L13} = 8$ A) respectively, where I_{Lh} is the h^{th} harmonic load current in amperes and V_{Sh} is the h^{th} harmonic source voltage in volts.

Table 3 presents the shunt STPF compensation simulated results using the proposed technique to account for the nonlinear loads. The optimal parameters of STPF (X_L and X_C) are subsequently found, these are dependent on the problem formulation. The system performance cases with shunt STPF installed at the load side confirms that different optimal solutions are obtained, satisfying all different criteria and constraints involved. Table 4 below, shows the levels of harmonic distortion and DPF after compensation. All resulting values appear well within the standard limits prescribed by IEEE Standard 519-2014 [39]. The objective function to minimize $NLCI$ limited the total harmonic distortion of the voltage to 5% and the values are all well within the IEEE 519-2014 standard limits

for the design of an STPF in all cases. It can be observed that all the tested orders of harmonics were reduced, including the low order harmonics (as can be seen in Figure 7 for case 2 and case 4).

Table 3. Simulated outcomes for the presented optimization approach.

$X_C (\Omega)$	$X_L (\Omega)$	PF (%)	η (%)	TL (kW)
Case 1				
4.11	0.40	99.75	99.36	10.61
Case 2				
4.11	0.40	99.45	99.36	10.67
Case 3				
4.19	0.27	99.38	99.66	5.76
Case 4				
5.06	0.28	95.54	99.63	6.16

Table 4. Harmonic distortions level and DPF after compensation for all cases under study.

Case	ITHD (%)	VTHD (%)	DPF (%)
1	3.18	1.37	99.81
2	8.05	3.19	99.81
3	3.21	0.77	99.43
4	15.29	2.89	96.69

The main merit of the presented approach is minimization of the *NLCI*, which is expected to reduce harmonics of the load voltage compared to an uncompensated system, even under the uncertainty of varying parameters. Moreover, placing more stringent requirements for voltage distortion reduction can benefit the level of harmonic current distortion. The simulation results highlight that the filter compensators can achieve the maximum *PF* (> 99%) in most cases. Figures 5 and 6 show *PF* and *TL* values before and after being compensated for all cases, respectively.

Transmission power losses can be reduced by correcting the power factor. Hence, the objective function of the filter design is subject to a constraint of $90\% \leq PF \leq 100\%$. For all case studies, Figures 5 and 6 show improvements in *PF* and reductions in transmission power losses respectively. For Figure 5 a reduction in transmission power losses for all case studies is attributed to the improvement in *PF*.

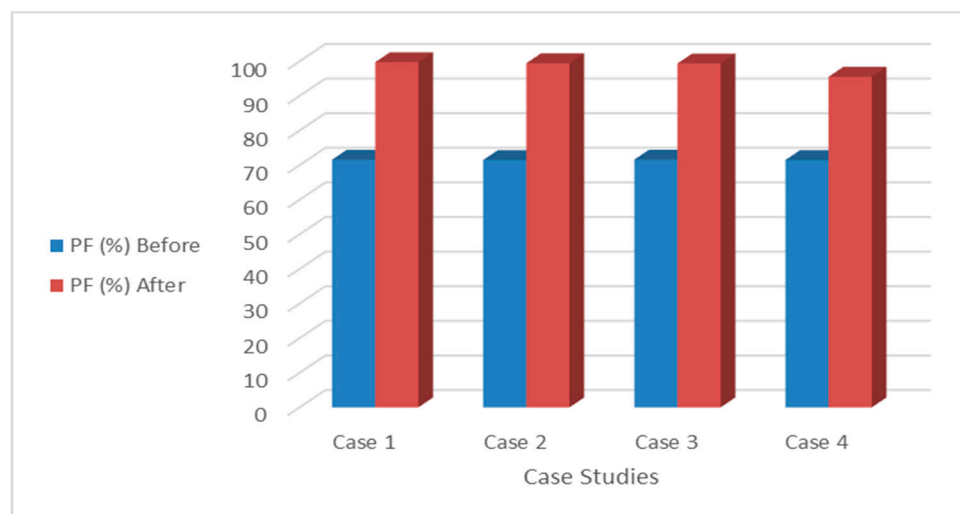


Figure 5. *PF* improvement across all case studies.

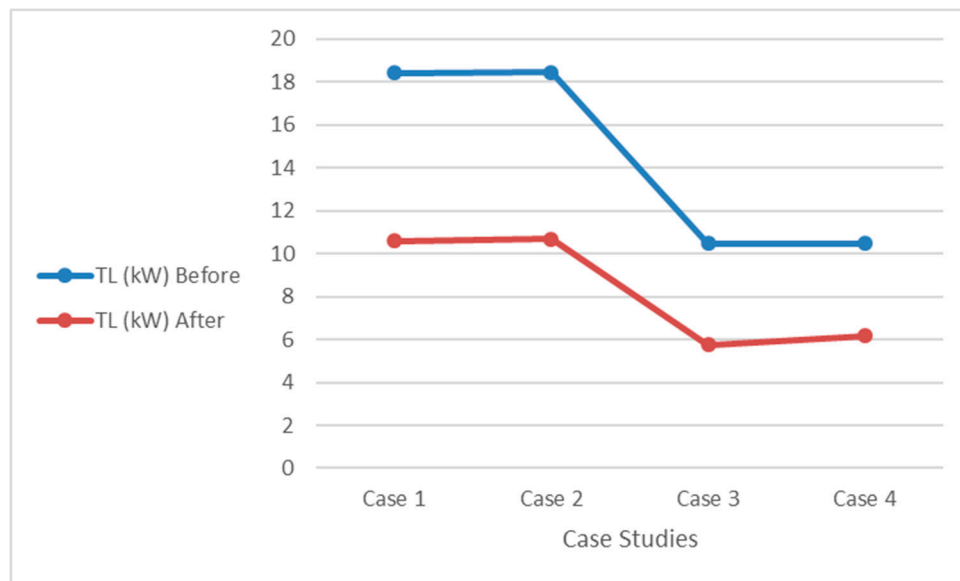


Figure 6. Reduction in Transmission Losses (TL) across all case studies.

Figure 7 shows a comparison of the *VTHD* results for the four case studies before compensation and after, when incorporating the objective function of minimizing *NLCI* as an objective function. Lower *VTHD* values are achieved in all the cases studied, showing the quality of the PCC voltage is also enhanced in each case. This is explained by an increase in the fundamental harmonic value of the voltage for all the case studies and leads to the conclusion that harmonic voltage components are considerably reduced, compared to the uncompensated components in each case. Figure 7 also shows clear improvements by reductions in all the tested load harmonic voltages, in cases 2 and 4, which follow from the application of our optimization method.

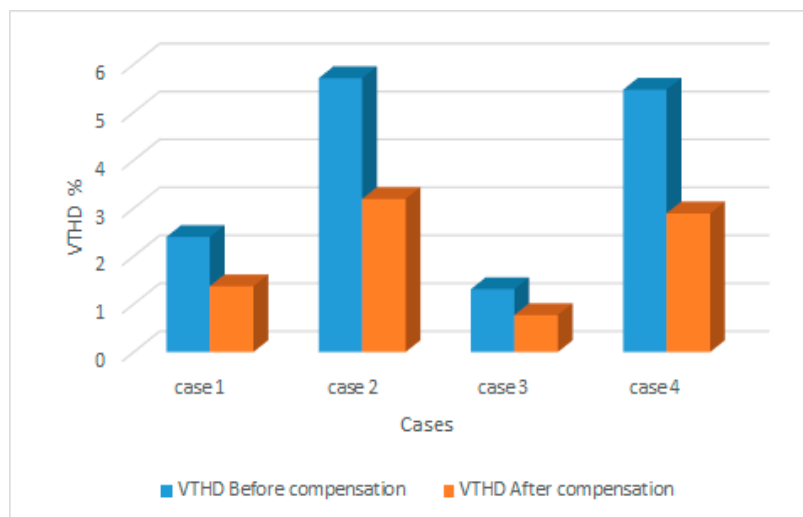


Figure 7. Improvement shown by reduction of the voltage harmonic distortion levels (*VTHD*) below the IEEE 519-2014 standard limits in all case studies, using *NLCI* as an objective function.

The proposed design of the shunt STPF results in an improvement in both the *PF* and *DPF* values in all cases. Furthermore, a notable decrease in the transmission losses, with a commensurate increase in the transmission efficiency of the compensated system, leads to a reduction in the rms value of the line current. This indicates that the system has become more linear after compensation with the optimally designed filter based on the *NLCI* objective function. As a result, the differences between the

rms value of the supply current and the rms value of the linear current are minimized, as calculated at the PCC.

Regarding capacitor loading constraints, Table 5 illustrates the calculated capacitor of the STPF duties for all cases under study. A comparison with the standard limits according to IEEE 18-2012 in the proposed design [38] validates the proposed approach.

Table 5. Capacitor duties calculation for all case studies.

Item	Calculated Values	Calculated (%)	IEEE 18-2012 Limit (%)	Exceeds Limit
Case 1				
V_C	2620.835	109.201	110	No
V_{CP}	2643.028	110.121	120	No
I_C	637.804	109.338	135	No
Q_C	1685.735	120.410	135	No
Case 2				
V_C	2621.056	109.211	110	No
V_{CP}	2674.345	111.431	120	No
I_C	639.361	109.605	135	No
Q_C	1709.871	122.134	135	No
Case 3				
V_C	2547.008	106.125	110	No
V_{CP}	2569.108	107.046	120	No
I_C	608.496	106.210	135	No
Q_C	1563.293	113.694	135	No
Case 4				
V_C	2508.601	104.525	110	No
V_{CP}	2640.681	110.028	120	No
I_C	506.375	106.840	135	No
Q_C	1337.174	117.554	135	No

6. Conclusions

A mathematical model has been developed and a solution presented for minimizing the non-linearity current index at the voltage load bus; this is aimed at maintaining the power factor of distribution circuits when subjected to nonlinear loads within accepted operational levels (above 90% or 95% PF [35]), using an STPF compensator.

The main contribution of this paper is the innovative adoption of the *NLCI* in an STPF to distinguish between the current due to the mains supply distortion and the nonlinear current due to the industrial user's loads. The user's load sourced nonlinear currents produce harmonic voltages as they pass through upstream power system impedance components, such as cables etc. The IEEE Recommended Practice and Requirements for Harmonic Control in Electrical Power Systems (IEEE 519-2014 standard) [36] states that harmonic currents should be reduced in order to minimize voltage harmonics. The passive filter which we propose, as designed by the proposed *NLCI* minimization approach, has proven its effectiveness by reducing harmonic currents and minimizing harmonic voltage distortion in standard power system models. Our methodology takes into account the IEEE 519-2014 guidelines, the capacitor loading expectations as defined in IEEE 18-2012, and the resonance conditions in the power system. This improves the correctness of the obtained solution and enhances the capability of the search algorithm to ensure convergence to the optimal solution. STPFs have been suggested for nonlinear loads due to their characteristic features, making them suitable to act as compensators to improve the *PF* for such nonlinear industrial loads. Furthermore, they prevent the spread of harmonic load currents into networks.

The simplest type of shunt passive filter is the single-tuned passive filter; it forms a short-circuit across the harmonic source at the tuned frequency. In this case, the harmonic current of this order will oscillate between the harmonic source and the passive filter. If there are multiple arms in the

single-tuned shunt filters, each of them will form a closed path with the harmonic source at its resonant frequency. In some cases, one single filter will be able to eliminate two or three harmonic orders simultaneously; these are called double-tuned filters or triple-tuned filters. However, they are more commonly used in HVDC systems rather than in other more common power system situations.

Standard passive filters are not suitable for varying power system conditions, since, once installed, they are fixed in place and have restricted operation as neither the tuned frequency nor the size of the filter can be changed easily. The passive elements in the filter are close-tolerance components, such that a change in the system operating conditions can lead to some detuning. Therefore, for routine operation, they require definite-purpose circuit breakers and special protective and monitoring devices. However, a well-designed, single-tuned passive filter has distinct advantages, including [2]:

1. Tolerance to high levels of MVar and almost maintenance-free service;
2. They are more economical to implement than their rotating counterparts;
3. A fast response time, of the order of one cycle or less, (which is particularly important in the presence of nonlinear loads).

The current paper tests a simple implementation of a newly designed single tuned passive filter, in model power systems with parameters selected to reflect IEEE standards and under typically experienced conditions. We recognize that real-world deployment would require, for example, additional filters (passive, active, or hybrid) and surge/transients protection (line reactors); however, this is beyond the scope of this paper.

Four cases of model power systems have been studied, with various configurations. Overall, all the performance indicators of the simulated results for the proposed method have been found to be satisfactory. This is illustrated by our results, which show that the newly designed filters assure that resonance is not introduced while maintaining objective functions within permissible limits for the power system, industrial customer's loads, and passive filter. In addition, the approach and suggested methodology presented provide a reduction in power line transmission losses, a reduction of harmonic distortion levels, and power factor improvement compared with other published solutions. Future approaches that will be explored within the context of filter design include the use of fractional order identification algorithms [44] to optimize the in situ responses of the designed filters and the use of descriptor representations for designing more complex RLC filters [45] with tailored responses.

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